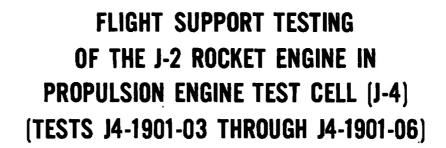
UNCLASSIFIED

AD NUMBER AD844885 LIMITATION CHANGES TO: Approved for public release; distribution is unlimited. FROM: Distribution authorized to DoD only; Administrative/Operational Use; DEC 1968. Other requests shall be referred to NASA Marshall Space Flight Center, Huntsville, AL. AUTHORITY AEDC ltr 12 Jul 1974

AEDC-TR-68-238

ARCHIVE COPY ... DO NOT LOAN

cy



N. R. Vetter and a constant and a co

December 1968

Each transmitted of this document outside the Department of Defense must have prior approval of NASA, Maschall Space Night Center (I-E-J), Huntsville, Alabama 35812.

LARGE ROCKET FACILITY

ARNOLD ENGINEERING DEVELOPMENT CENTER

AIR FORCE SYSTEMS COMMAND

ARNOLD AIR FORCE STATION, TENNESSEE

PROPERTY OF U. S. ALR FCECE AUGO LINGURY F40300-S9-C-0001





NOTICES

-- --

When U. S. Government drawings specifications, or other data are used for any purpose other than a definitely related Government procurement operation, the Government thereby incurs no responsibility nor any obligation whatsoever, and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise, or in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

Qualified users may obtain copies of this report from the Defense Documentation Center.

References to named commercial products in this report are not to be considered in any sense as an endorsement of the product by the United States Air Force or the Government.

FLIGHT SUPPORT TESTING OF THE J-2 ROCKET ENGINE IN PROPULSION ENGINE TEST CELL (J-4) (TESTS J4-1901-03 THROUGH J4-1901-06)

N. R. Vetter ARO, Inc.

This document has been approved for public releases to the state of th

Each transmittal of this document outside the Department of Defense must have prior approval of NASA, Marshall Space Flight Center (I-E-J), Huntsville, Mabama 35812.

FOREWORD

The work reported herein was sponsored by the National Aeronautics and Space Administration (NASA), Marshall Space Flight Center (MSFC) (I-E-J), under System 921E, Project 9194.

The results of the tests presented were obtained by ARO, Inc., (a subsidiary of Sverdrup & Parcel and Associates, Inc.), contract operator of the Arnold Engineering Development Center (AEDC), Air Force Systems Command (AFSC), Arnold Air Force Station, Tennessee, under Contract F40600-69-C-0001. Program direction was provided by NASA/MSFC; engineering liaison was provided by North American Rockwell Corporation, Rocketdyne Division, manufacturer of the J-2 rocket engine, and McDonnell Douglas Corporation, Douglas Aircraft Company, Missile and Space Systems Division, manufacturer of the S-IVB stage. The testing reported herein was conducted between July 23 and August 15, 1968, in Propulsion Engine Test Cell (J-4) of the Large Rocket Facility (LRF) under ARO Project No. KA1901. The manuscript was submitted for publication on September 25, 1968.

Information in this report is embargoed under the Department of State International Traffic in Arms Regulations. This report may be released to foreign governments by departments or agencies of the U. S. Government subject to approval of NASA, Marshall Space Flight Center (I-E-J), or higher authority. Private individuals or firms require a Department of State export license.

This technical report has been reviewed and is approved.

Edgar D. Smith
Major, USAF
AF Representative, LRF
Directorate of Test

Roy R. Croy, Jr. Colonel, USAF Director of Test

ABSTRACT

Fourteen firings of the Rocketdyne J-2 rocket engine (S/N J-2036-1) we're conducted at pressure altitude conditions during four test periods (J4-1901-03 through J4-1901-06) between July 23 and August 15, 1968, in Test Cell J-4 of the Large Rocket Facility. This testing was in support of the J-2 engine application to the S-II and S-IVB stages of the Saturn V vehicle. The firings were accomplished at pressure altitudes between 78,000 and 110,000 ft at engine start. The primary objective of these firings was to evaluate engine start transients under various combinations of starting conditions with start tank energy being the major variable. The total accumulated firing duration for these four test periods was 223.2 sec.

t sage i George Etchiologi G

Çirga ili. Birlina

This document is subject to special export controls and each transmittal to foreign governments of foreign nationals may be made only with prior approval of NASA, Marshall Space Flight Center (I-E-J), Huntsville, Alabama 35812.

This document has been approved for public release its distribution is unlimited. Re. A.F. Lell

CONTENTS

			Page
		ABSTRACT	iii
_		NOMENCLATURE	ix
I. II.		NTRODUCTION	1 1
Π	_	PROCEDURE	7
IV	-	RESULTS AND DISCUSSION	8
V	-	SUMMARY OF RESULTS	17
	F	REFERENCES	17
		APPENDIXES	
I.	IL	LUSTRATIONS	
Fi	gur	<u>e</u>	
	1.	Test Cell J-4 Complex	21
	2.	Test Cell J-4, Artist's Conception	22
	3.	Engine Details	23
	4.	S-IVB Battleship Stage/J-2 Engine Schematic	24
	5.	Engine Schematic	25
	6.	Engine Start Logic Schematic	26
	7.	Engine Start and Shutdown Sequence	27
	8.	Engine Start Conditions for the Pump Inlets, Start Tank, and Helium Tank	29
	•		20
	9.	Thermal Conditioning History of Engine Components, Firing 03A	31
	10.	Engine Transient Operation, Firing 03A	32
	11.	Fuel Pump Start Transient Performance, Firing 03A	36
	12.	Engine Ambient and Combustion Chamber Pressure, Firing 03A	37
	13.	Thermal Conditioning History of Engine Components, Firing 03B	38
	14.	Engine Transient Operation, Firing 03B	39

AEDC-TR-68-238

Figure		Page
15.	Fuel Pump Start Transient Performance, Firing 03B	43
.16.	Engine Ambient and Combustion Chamber Pressure, Firing 03B	44
17.	Thermal Conditioning History of Engine Components, Firing 03C	45
18.	Engine Transient Operation, Firing 03C	46
19.	Fuel Pump Start Transient Performance, Firing 03C	50
20.	Engine Ambient and Combustion Chamber Pressure, Firing 03C	5 1 [.]
21.	Thermal Conditioning History of Engine Components, Firing 03D	52
22.	Engine Transient Operation, Firing 03D	53
23.	Fuel Pump Start Transient Performance, Firing 03D	55
24.	Engine Ambient and Combustion Chamber Pressure, Firing 03D	56
25.	Thermal Conditioning History of Engine Components, Firing 04A	57
26.	Engine Transient Operation, Firing 04A	58
27.	Fuel Pump Start Transient Performance, Firing 04A	62
28.	Engine Ambient and Combustion Chamber Pressure, Firing 04A	63
29.	Thermal Conditioning History of Engine Components, Firing 04B	. 64
30.	Engine Transient Operation, Firing 04B	65
31.	Fuel Pump Start Transient Performance, Firing 04B	69
32.	Engine Ambient and Combustion Chamber Pressure, Firing 04B	70
33.	Thermal Conditioning History of Engine Components, Firing 04C	71
34.	Engine Transient Operation, Firing 04C	72
35.	Fuel Pump Start Transient Performance, Firing 04C	76
36.	Engine Ambient and Combustion Chamber Pressure, Firing 04C	77

Figure		Page
37.	Thermal Conditioning History of Engine Components, Firing 04D	78
38.	Engine Transient Operation, Firing 04D	79
39.	Fuel Pump Start Transient Performance, Firing 04D	81
40.	Engine Ambient and Combustion Chamber Pressure, Firing 04D	82
41.	Thermal Conditioning History of Engine Components, Firing 05A	83
42.	Engine Transient Operation, Firing 05A	84
43.	Engine Ambient and Combustion Chamber Pressure, Firing 05A	86
44.	Thermal Conditioning History of Engine Components, Firing 06A	87
45.	Engine Transient Operation, Firing 06A	88
4 6.	Fuel Pump Start Transient Performance, Firing 06A	92
47. :	Engine Ambient and Combustion Chamber Pressure, Firing 06A	93
48.	Thermal Conditioning History of Engine Components, Firing 06B	94
49.	Engine Transient Operation, Firing 06B	95
50.	Fuel Pump Start Transient Performance, Firing 06B	99
51.	Engine Ambient and Combustion Chamber Pressure, Firing 06B	100
52.	Thermal Conditioning History of Engine Components, Firing 06C	101
53.	Engine Transient Operation, Firing 06C	102
54.	Fuel Pump Start Transient Performance, Firing 06C	106
55.	Engine Ambient and Combustion Chamber Pressure, Firing 06C	107
56.	Thermal Conditioning History of Engine Components, Firing 06D	108
57.	Engine Transient Operation, Firing 06D	109
58.	Fuel Pump Start Transient Performance, Firing 06D	113

AEDC-TR-68-238

Figure			Page
59.		gine Ambient and Combustion Chamber Pressure, ring 06D	114
60.		ermal Conditioning History of Engine Components, ring 06E	115
61.	Eng	gine Transient Operation, Firing 06E	116
62.	Fue	el Pump Start Transient Performance, Firing 06E	118
63.	•	gine Ambient and Combustion Chamber Pressure, ring 06E	119
II. T	ABL	ES .	;
	I.	Major Engine Components	120
	II.	Summary of Engine Orifices	121
.]	III.	Engine Modifications (Between Tests J4-1901-03 and J4-1901-06)	122
]	IV.	Engine Component Replacements (Between Tests J4-1901-03 and J4-1901-06)	122
	v.	Engine Purge and Component Conditioning Sequence	123
•	VI.	Summary of Test Requirements and Results	124
V	⁄Π.	Engine Valve Timings	127
V	III.	Engine Performance Summary	129
III. IN	ISTE	RUMENTATION	130
		HOD OF CALCULATION (PERFORMANCE	143

NOMENCLATURE

A Area, in.²

_4.4

. ; .

ASI Augmented spark igniter

ES Engine start, designated as the time that helium control and

ignition phase solenoids are energized

GG Gas generator

MOV Main oxidizer valve

STDV Start tank discharge valve

to Defined as the time at which the opening signal is applied to

the start tank discharge valve solenoid

VSC Vibration safety counts, defined as the time at which engine

vibration was in excess of 150 g rms in a 960- to 6000-Hz

frequency range

SUBSCRIPTS

f Force

m Mass

t Throat

SECTION I

Testing of the Rocketdyne J-2 rocket engine using an S-IVB battleship stage has been in progress since July, 1966, at AEDC in support of J-2 engine application on the Saturn IB and Saturn V launch vehicles for the NASA Apollo Program. The 14 firings reported herein were conducted during test periods J4-1901-03 through J4-1901-06 in Propulsion Engine Test Cell (J-4) (Figs. 1 and 2, Appendix I) of the Large Rocket Facility (LRF). These firings were to investigate engine start transients for S-IVB first burn and 80-min orbital restarts and S-II starts utilizing a 230,000-lbf-thrust configuration engine. The firings were accomplished at pressure altitudes ranging from 78,000 to 110,000 ft (geometric pressure altitude, Z, Ref. 1) at engine start. Engine components were conditioned to temperatures predicted for an S-IVB first burn, 80-min restart, or S-II start. Data collected to accomplish the test objectives are presented herein. The results of the previous test period are presented in Ref. 2.

SECTION-II APPARATUS

2.1 TEST ARTICLE

The test article was a J-2 rocket engine (Fig. 3) designed and developed by Rocketdyne Division of North American Rockwell Corporation. The engine uses liquid oxygen and liquid hydrogen as propellants and has a thrust rating of 230,000 lbf at an oxidizer-to-fuel mixture ratio of 5.5. An S-IVB battleship stage was used to supply propellants to the engine. A schematic of the battleship stage is presented in Fig. 4.

Listings of major engine components and engine orifices for this test period are presented in Tables I and II, respectively (Appendix II). All engine modifications and component replacements performed since the previous test period are presented in Tables III and IV, respectively.

2.1.1 J-2 Rocket Engine

The J-2 rocket engine (Figs. 3 and 5, Ref. 3) features the following major components:

- 1. Thrust Chamber The tubular-walled, bell-shaped thrust chamber consists of an 18.6-in.-diam combustion chamber (8.0 in. long from the injector mounting to the throat inlet) with a characteristic length (L*) of 24.6 in., a 170.4-in.² throat area, and a divergent nozzle with an expansion ratio of 27.1. Thrust chamber length (from the injector flange to the nozzle exit) is 107 in. Cooling is accomplished by the circulation of engine fuel flow downward from the fuel manifold through 180 tubes and then upward through 360 tubes to the injector.
- 2. Thrust Chamber Injector The injector is a concentric-orificed (concentric fuel orifices around the oxidizer post orifices), porous-faced injector. Fuel and oxidizer injector orifice areas are 25.0 and 16.0 in.², respectively. The porous material, forming the injector face, allows approximately 3.5 percent of total fuel flow to transpiration cool the face of the injector.
- 3. Augmented Spark Igniter The augmented spark igniter unit is mounted on the thrust chamber injector and supplies the initial energy source to ignite propellants in the main combustion chamber. The augmented spark igniter chamber is an integral part of the thrust chamber injector. Fuel and oxidizer are ignited in the combustion area by two spark plugs.
- 4. Fuel Turbopump The turbopump is composed of a two-stage turbine-stator assembly, an inducer, and a seven-stage axial-flow pump. The pump is self lubricated and nominally produces, at rated conditions, a head rise of 38,215 ft (1248 psia) of liquid hydrogen at a flow rate of 8585 gpm for a rotor speed of 27,265 rpm.
- 5. Oxidizer Turbopump The turbopump is composed of a two-stage turbine-stator assembly and a single-stage centrifugal pump. The pump is self lubricated and nominally produces, at rated conditions, a head rise of 2170 ft (1107 psia) of liquid oxygen at a flow rate of 2965 gpm for a rotor speed of 8688 rpm.
- 6. Gas Generator The gas generator consists of a combustion chamber containing two spark plugs, a pneumatically operated control valve containing oxidizer and fuel poppets, and an injector assembly. The oxidizer and fuel poppets provide a fuel lead to the gas generator combustion chamber. The high energy gases produced by the gas generator are directed to the fuel

- turbine and then to the oxidizer turbine (through the turbine crossover duct) before being exhausted into the thrust chamber at an area ratio (A/A_t) of approximately 11.
- 7. Propellant Utilization Valve The motor-driven propellant utilization valve is mounted on the oxidizer turbopump and bypasses liquid oxygen from the discharge to the inlet side of the pump to vary engine mixture ratio.
- 8. Propellant Bleed Valves The pneumatically operated fuel and oxidizer bleed valves provide pressure relief for the boiloff of propellants trapped between the battleship stage prevalves and main propellant valves at engine shutdown.
- 9. Integral Hydrogen Start Tank and Helium Tank The integral tanks consist of a 7258-in.³ sphere for hydrogen with a 1000-in.³ sphere for helium located within it. Pressurized gaseous hydrogen in the start tank provides the initial energy source for spinning the propellant turbopumps during engine start. The helium tank provides a helium pressure supply to the engine pneumatic control system.
 - 10. Oxidizer Turbine Bypass Valve The pneumatically actuated oxidizer turbine bypass valve provides control of the fuel turbine exhaust gases directed to the oxidizer turbine in order to control the oxidizer-to-fuel turbine spinup relationship. The fuel turbine exhaust gases which bypass the oxidizer turbine are discharged into the thrust chamber.
 - 11. Main Oxidizer Valve The main oxidizer valve is a pneumatically actuated, two-stage, butterfly-type valve located in the oxidizer high pressure duct between the turbopump and main injector. The first-stage actuator positions the main oxidizer valve at the 14-deg position to obtain initial thrust chamber ignition; the second-stage actuator ramps the main oxidizer valve full open to accelerate the engine to main-stage operation.
 - 12. Main Fuel Valve The main fuel valve is a pneumatically actuated butterfly-type valve located in the fuel high pressure duct between the turbopump and the fuel manifold.
 - 13. Pneumatic Control Package The pneumatic control package controls all pneumatically operated engine valves and purges.
 - 14. Electrical Control Assembly The electrical control assembly provides the electrical logic required for proper sequencing of engine components during operation.

15. Primary and Auxiliary Flight Instrumentation Packages - The instrumentation packages contain sensors required to monitor critical engine parameters. The packages provide environmental control for the sensors.

2.1.2 S-IVB Battleship Stage

The S-IVB battleship stage is approximately 22 ft in diameter and 49 ft long and has a maximum propellant capacity of 46,000 lb of liquid hydrogen and 199,000 lb of liquid oxygen. The propellant tanks, fuel above oxidizer, are separated by a common bulkhead. Propellant prevalves, in the low pressure ducts (external to the tanks) interfacing the stage and the engine, retain propellant in the stage until being admitted into the engine to the main propellant valves and serve as emergency engine shutoff valves. Propellant recirculation pumps in both fuel and oxidizer tanks are utilized to circulate propellants through the low pressure ducts and turbopumps before engine start to stabilize hardware temperatures near normal operating levels and to prevent propellant temperature stratification. Vent and relief valve systems are provided for both propellant tanks.

Pressurization of the fuel and oxidizer tanks was accomplished by facility systems using hydrogen and helium, respectively, as the pressurizing gases. The engine-supplied gaseous hydrogen for fuel tank pressurization during S-IVB and S-II flight was routed to the facility venting system.

2.2 TEST CELL

Test Cell J-4, Fig. 2, is a vertically oriented test unit designed for static testing of liquid-propellant rocket engines and propulsion systems at pressure altitudes of 100,000 ft. The basic cell construction provides a 1.5-million-lbf-thrust capacity. The cell consists of four major components (1) test capsule, 48 ft in diameter and 82 ft in height, situated at grade level and containing the test article; (2) spray chamber, 100 ft in diameter and 250 ft in depth, located directly beneath the test capsule to provide exhaust gas cooling and dehumidification; (3) coolant water, steam, nitrogen (gaseous and liquid), hydrogen (gaseous and liquid), and liquid oxygen and gaseous helium storage and delivery systems for operation of the cell and test article; and (4) control building, containing test article controls, test cell controls, and data acquisition equipment. Exhaust machinery is connected with the spray chamber and maintains a minimum test cell pressure before and after the engine firing and exhausts the products of combustion from the

engine firing. Before a firing, the facility steam ejector, in series with the exhaust machinery, provides a pressure altitude of 100,000 ft in the test capsule. A detailed description of the test cell is presented in Ref. 4.

The battleship stage and the J-2 engine were oriented vertically downward on the centerline of the diffuser-steam ejector assembly. This assembly consisted of a diffuser duct (20 ft in diameter by 150 ft in length), a centerbody steam ejector within the diffuser duct, a diffuser insert (13.5 ft in diameter by 30 ft in length) at the inlet to the diffuser duct, and a gaseous nitrogen annular ejector above the diffuser insert. The diffuser insert was provided for dynamic pressure recovery of the engine exhaust gases and to maintain engine ambient pressure altitude (attained by the steam ejector) during the engine firing. The annular ejector was provided to suppress steam recirculation into the test capsule during steam ejector shutdown. The test cell was also equipped with (1) a gaseous nitrogen purge system for continuously inerting the normal air in-leakage of the cell; (2) a gaseous nitrogen repressurization system for raising test cell pressure, after engine cutoff, to a level equal to spray chamber pressure and for rapid emergency inerting of the capsule; and (3) a spray chamber liquid nitrogen supply and distribution manifold for initially inerting the spray chamber and exhaust ducting and for increasing the molecular weight of the hydrogenrich exhaust products.

An engine component conditioning system was provided for temperature conditioning engine components. The conditioning system utilized a liquid hydrogen-helium heat exchanger to provide cold helium gas for component conditioning. Engine components requiring temperature conditioning were the thrust chamber, crossover duct, start tank discharge valve (test 05 only), and main oxidizer valve second-stage actuator. Helium was routed internally through the crossover duct and tubular-walled thrust chamber and externally over the start tank discharge valve. Main oxidizer valve conditioning was achieved by opening the prevalves and permitting propellants into the engine.

2.3 INSTRUMENTATION

Instrumentation systems were provided to measure engine, stage, and facility parameters. The engine instrumentation was comprised of (1) flight instrumentation for the measurement of critical engine parameters and (2) facility instrumentation which was provided to verify the flight instrumentation and to measure additional engine parameters. The flight instrumentation was provided and calibrated by the engine manufacturer; facility instrumentation was initially calibrated and periodically

recalibrated at AEDC. Appendix III contains a list of all measured test parameters and the locations of selected sensing points.

Pressure measurements were made using strain-gage and capacitance-type pressure transducers. Temperature measurements were made using resistance temperature transducers and thermocouples. Oxidizer and fuel turbopump shaft speeds were sensed by magnetic pick-up. Fuel and oxidizer flow rates to the engine were measured by turbine-type flowmeters which are an integral part of the engine. The propellant recirculation flow rates were also monitored with turbine-type flowmeters. Vibrations were measured by accelerometers mounted on the oxidizer injector dome and on the turbopumps. Primary engine and stage valves were instrumented with linear potentiometers and limit switches.

The data acquisition systems were calibrated by (1) precision electrical shunt resistance substitution for the pressure transducers and resistance temperature transducer units; (2) voltage substitution for the thermocouples; (3) frequency substitution for shaft speeds and flowmeters; and (4) frequency-voltage substitution for accelerometers.

The types of data acquisition and recording systems used during this test period were (1) a multiple-input digital data acquisition system (Microsadic®) scanning each parameter at 40 samples per second and recording on magnetic tape; (2) single-input, continuous-recording FM systems recording on magnetic tape; (3) photographically recording galvanometer oscillographs; (4) direct-inking, null-balance potentiometer-type X-Y plotters and strip charts; and (5) optical data recorders. Applicable systems were calibrated before each test (atmospheric and altitude calibrations). Television cameras, in conjunction with video tape recorders, were used to provide visual coverage during an engine firing, as well as for replay capability for immediate examination of unexpected events.

2.4 CONTROLS

Control of the J-2 engine, battleship stage, and test cell systems during the terminal countdown was provided from the test cell control room. A facility control logic network was provided to interconnect the engine control system, major stage systems, the engine safety cutoff system, the observer cutoff circuits, and the countdown sequencer. A schematic of the engine start control logic is presented in Fig. 6. The sequence of engine events for a normal start and shutdown is presented in Figs. 7a and b. Two control logics for sequencing the stage prevalves

and recirculation systems with engine start for simulating engine flight start sequences are presented in Figs. 7c and d.

SECTION III PROCEDURE

٠.

Preoperational procedures were begun several hours before the test period. All consumable storage systems were replenished, and engine inspections, leak checks, and drying procedures were conducted. Propellant tank pressurants and engine pneumatic and purge gas samples were taken to ensure that specification requirements were met. Chemical analysis of propellants was provided by the propellant suppliers. Facility sequence, engine sequence, and engine abort checks were conducted within a 24-hr time period before an engine firing to verify the proper sequence of events. Facility and engine sequence checks consisted of verifying the timing of valves and events to be within specified limits; the abort checks consisted of electrically simulating engine malfunctions to verify the occurrence of an automatic engine cutoff signal. A final engine sequence check was conducted immediately preceding the test period.

Oxidizer dome, gas generator oxidizer injector, and thrust chamber jacket purges were initiated before evacuating the test cell. After completion of instrumentation calibrations at atmospheric conditions, the test cell was evacuated to approximately 0.5 psia with the exhaust machinery, and instrumentation calibrations at altitude conditions were conducted. Immediately before loading propellants on board the vehicle, the cell and exhaust-ducting atmosphere was inerted. At this same time, the cell nitrogen purge was initiated for the duration of the test period, except for the engine firing. The vehicle propellant tanks were then loaded, and the remainder of the terminal countdown was conducted. Temperature conditioning of the various engine components was accomplished as required, using the facility-supplied engine component conditioning system. Engine components which required temperature conditioning were the thrust chamber, the crossover duct, start tank discharge valve (test 05 only), and main oxidizer valve second-stage actuator. Table V presents the engine purges and thermal conditioning operations during the terminal countdown and immediately following the engine firing.

SECTION IV RESULTS AND DISCUSSION

4 1 TEST SUMMARY

Fourteen firings of the Rocketdyne J-2 rocket engine (J-2036-1) were conducted on July 23 and 31 and August 8 and 15, 1968, during test periods J4-1901-03 through J4-1901-06. These firings were in support of the S-II/S-V and S-IVB/S-V J-2 engine application and flight support testing. Testing was accomplished at pressure altitudes ranging from 78,000 to 110,000 ft at engine start.

Test requirements and specific test results are summarized in Table VI. Start and shutdown transient operating times for selected engine valves are presented in Table VII. Figure 8 shows engine start conditions for pump inlets and start and helium tanks. The total firing duration for the four test periods was 223.2 sec. Calculated engine performance for the five 32.5-sec duration firings is presented in Table VIII. Methods of calculations shown are presented in Appendix IV. Specific test objectives and a brief summary of each firing are presented below.

Firing	Test Objectives	Results
03A	Simulate S-IVB first burn to evaluate augmented spark igniter ignition characteristics.	Augmented spark igniter ignition was detected at $t_0 + 0.222$ sec. Thrust chamber ignition occurred at $t_0 + 0.979$ sec.
03B	Simulate S-IVB 80-min restart with maximum start tank energy and low fuel pump inlet pressure.	Thrust chamber ignition occurred at $t_0 + 0.961$ sec, and thrust chamber pressure reached 550 psia at $t_0 + 1.993$ sec. Gas generator outlet temperature first peak was 1750°F with a second peak of 1930°F.
03C	Simulate S-IVB first burn to evaluate maximum gas generator outlet temperature first peak.	Gas generator outlet temperature first peak was 1640°F.

Firing	Test Objectives	Results
03D	Repeat firing 03B with start tank gas 50°F colder.	Thrust chamber ignition occurred at t ₀ + 0.939 sec. Gas generator outlet temperature first peak was 2000°F with a second peak of 2190°F. Firing was terminated at t ₀ + 1.264 sec by engine safety cutoff system.
04A	Simulate S-IVB first burn to evaluate engine start transient with maximum start tank energy and warmest thrust chamber.	Thrust chamber ignition occurred at t0 + 0.962 sec, and thrust chamber pressure reached 550 psia at t0 + 1.821 sec. Gas generator outlet temperature first peak was 1870°F.
04B 	Simulate S-IVB 80-min restart to evaluate gas generator out- let temperature transient with minimum start tank tempera- ture.	Gas generator outlet temperature first peak was 1940°F, and the second peak was 2120°F.
04C	Simulate S-IVB first burn to evaluate augmented spark igniter ignition and gas generator outlet temperature transient with maximum start tank energy and propellant pump inlet pressures.	Augmented spark igniter ignition was detected 0.210 sec after engine start. Gas generator outlet temperature first peak was 1960°F.
04D	Simulate S-IVB 80-min restart to evaluate augmented spark igniter ignition and gas generator outlet temperature transient with maximum starting energy.	Augmented spark igniter ignition was detected 0.260 sec after engine start. Gas generator outlet temperature first peak was 2010°F, and the second peak was 2160°F.
05A	Simulate S-II firing to evaluate augmented spark igniter ignition with minimum augmented spark igniter mixture ratio, maximum fuel pump inlet pressure, and warmest thrust chamber.	There was no indication of augmented spark igniter ignition before main-stage control solenoid "on" command, at which time the firing was terminated by the engine logic.

Firing	Test Objectives	Results
06A	Simulate S-IVB 6-hr restart to evaluate engine start characteristics with minimum starting energy.	Thrust chamber ignition occurred at $t_0 + 1.091$ sec, and thrust chamber pressure reached 550 psia at $t_0 + 3.233$ sec. Gas generator outlet temperature first peak was 1450° F.
06B	Simulate S-IVB 80-min restart to evaluate gas generator out- let temperature transient with minimum start tank tempera- ture.	Gas generator outlet temperature first peak was 1730°F, and the second peak was 1760°F.
06C	Simulate S-IVB first burn to evaluate engine start characteristics with minimum starting energy.	Thrust chamber ignition occurred at $t_0 + 1.062$ sec, and thrust chamber pressure reached 550 psia at $t_0 + 2.124$ sec. Gas generator outlet temperature first peak was $2020^{\circ}F$.
06D	Simulate S-IVB 80-min restart to evaluate gas generator outlet temperature transient with minimum start tank and thrust chamber temperature.	Gas generator outlet temperature first peak was 1930°F. There was no second peak.
06E	Determine the effect of a -200°F oxidizer injector dome on start transient combustion stability with starting conditions similar to firing 06A.	Total vibration safety counts duration was less than 10 msec before engine cutoff command.

4.2 TEST RESULTS

4.2.1 Firing J4-1901-03A

The programmed 32.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 9. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 10. Fuel pump start transient performance

is shown in Fig. 11. Pressure altitude at engine start was 100,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 12.

Test conditions were selected to simulate an S-IVB first burn. Augmented spark igniter ignition was detected at $t_0 + 0.222$ sec. Thrust chamber ignition (chamber pressure attains 100 psia) occurred at $t_0 + 0.979$ sec, and chamber pressure reached 550 psia at $t_0 + 1.848$ sec. Engine vibration in excess of 150 g occurred for 20 msec beginning at $t_0 + 0.978$ sec. Gas generator outlet temperature first peak was 1560°F with no second peak.

4.2.2 Firing J4-1901-03B

The programmed 7.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 13. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 14. Fuel pump start transient performance is shown in Fig. 15. Pressure altitude at engine start was 106,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 16.

Test conditions were selected to simulate an S-IVB 80-min restart with maximum start tank energy. Augmented spark igniter ignition was detected 0.248 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.961$ sec, and chamber pressure reached 550 psia at $t_0 + 1.993$ sec. Engine vibration in excess of 150 g occurred for 6 msec beginning at $t_0 + 0.960$ sec. Gas generator outlet temperature first peak was 1750°F with a second peak of 1930°F.

4.2.3 Firing J4-1901-03C

The programmed 32.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 17. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 18. Fuel pump start transient performance is shown in Fig. 19. Pressure altitude at engine start was 106,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 20.

Test conditions were selected to simulate an S-IVB first burn with a worst-case gas generator outlet temperature first peak. Augmented spark igniter ignition was detected 0.162 sec after engine start. Thrust chamber ignition occurred at $t_0 + 1.073$ sec, and chamber pressure reached 550 psia at $t_0 + 1.951$ sec. Engine vibration in excess of 150 g occurred for 35 msec beginning at $t_0 + 0.964$ sec. Gas generator outlet temperature first peak was 1640° F with no second peak.

4.2.4 Firing J4-1901-03D

The programmed 7.5-sec duration firing was terminated at $t_0 + 1.264$ sec by the engine safety cutoff system because of excessive gas generator outlet temperature. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 21. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 22. Fuel pump start transient performance is shown in Fig. 23. Pressure altitude at engine start was 104,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 24.

Test conditions were selected to repeat firing 03B with start tank gas $50^{\circ}F$ colder. Augmented spark igniter ignition was detected 0.212 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.939$ sec. Engine vibration in excess of 150 g occurred for 5 msec beginning at $t_0 + 0.945$ sec. Gas generator outlet temperature first peak was $2000^{\circ}F$ with a second peak of $2190^{\circ}F$.

4.2.5 Firing J4-1901-04A

The programmed 32.5-sec duration firing was terminated at $t_0 + 25.02$ sec by the inadvertent opening (resulting from incorrect procedure) of the thrust chamber purge valve. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 25. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 26. Fuel pump start transient performance is shown in Fig. 27. Pressure altitude at engine start was 78,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 28.

Test conditions were selected to simulate an S-IVB first burn with maximum start tank energy and the warmest expected thrust chamber. Augmented spark igniter ignition was detected 0.243 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.962$ sec, and chamber

pressure reached 550 psia at $t_0+1.821$ sec. Engine vibration in excess of 150 g occurred for 5 msec beginning at $t_0+0.978$ sec. Gas generator outlet temperature first peak was $1870^{\circ}F$ with a second peak of $1750^{\circ}F$.

4.2.6 Firing J4-1901-04B

The programmed 7.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 29. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 30. Fuel pump start transient performance is shown in Fig. 31. Pressure altitude at engine start was 100,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 32.

Test conditions were selected to simulate an S-IVB 80-min restart with minimum start tank temperature. Augmented spark igniter ignition was detected 0.180 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.945$ sec, and chamber pressure reached 550 psia at $t_0 + 2.005$ sec. Engine vibration in excess of 150 g occurred for 15 msec beginning at $t_0 + 1.046$ sec. Gas generator outlet temperature first peak was $1940^{\circ}F$ with a second peak of $2120^{\circ}F$.

4.2.7 Firing J4-1901-04C

The programmed 32.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 33. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 34. Fuel pump start transient performance is shown in Fig. 35. Pressure altitude at engine start was 100,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 36.

Test conditions were selected to simulate an S-IVB first burn with maximum starting energy and maximum propellant pump inlet pressures. Augmented spark igniter ignition was detected 0.210 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.958$ sec, and chamber pressure reached 550 psia at $t_0 + 1.807$ sec. Engine vibration in excess of 150 g occurred for 26 msec beginning at $t_0 + 0.956$ sec. Gas generator outlet temperature first peak was $1960^{\circ}F$ with no second peak.

4.2.8 Firing J4-1901-04D

The programmed 2.0-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 37. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 38. Fuel pump start transient performance is shown in Fig. 39. Pressure altitude at engine start was 100,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 40.

Test conditions were selected to simulate an S-IVB 80-min restart with maximum starting energy. Augmented spark igniter ignition was detected 0.260 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.948$ sec, and chamber pressure reached 550 psia at $t_0 + 1.984$ sec. Engine vibration in excess of 150 g occurred for 9 msec beginning at $t_0 + 0.948$ sec. Gas generator outlet temperature first peak was 2010° F with a second peak of 2160° F.

4.2.9 Firing J4-1901-05A

The programmed 32.5-sec duration firing was terminated at $t_0 + 0.448$ sec (main-stage command) by the engine logic because augmented spark igniter ignition had not been detected. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 41. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 42. Pressure altitude at engine start was 104,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 43.

Test conditions were selected to simulate an S-II firing with minimum augmented spark igniter mixture ratio, maximum fuel pump inlet pressure, and warmest expected thrust chamber.

4.2.10 Firing J4-1901-06A

The programmed 32.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 44. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 45. Fuel pump start transient performance is shown in Fig. 46. Pressure altitude at engine start was 89,000 ft.

Engine ambient and combustion chamber pressure histories are shown in Fig. 47.

Test conditions were selected to simulate an S-IVB 6-hr orbital coast restart with minimum starting energy. Augmented spark igniter ignition was detected 0.362 sec after engine start. Thrust chamber ignition occurred at $t_0 + 1.091$ sec, and chamber pressure reached 550 psia at $t_0 + 3.233$ sec. Engine vibration in excess of 150 g occurred for 75 msec beginning at $t_0 + 1.054$ sec. Gas generator outlet temperature first peak was $1450^{\circ}\mathrm{F}$ with no second peak.

4.2.11 Firing J4-1901-06B

The programmed 7.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 48. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 49. Fuel pump start transient performance is shown in Fig. 50. Pressure altitude at engine start was 99,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 51.

Test conditions were selected to simulate an S-IVB 80-min restart with minimum start tank temperature. Augmented spark igniter ignition was detected 0.235 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.953$ sec, and chamber pressure reached 550 psia at $t_0 + 2.013$ sec. Engine vibration in excess of 150 g occurred for 21 msec beginning at $t_0 + 0.950$ sec. Gas generator outlet temperature first peak was 1730°F with a second peak of 1760°F.

4.2.12 Firing J4-1901-06C

The programmed 32.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 52. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 53. Fuel pump start transient performance is shown in Fig. 54. Pressure altitude at engine start was 103,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 55.

Test conditions were selected to simulate an S-IVB first burn with minimum starting energy. Augmented spark igniter ignition was

detected 0.242 sec after engine start. Thrust chamber ignition occurred at $t_0 + 1.062$ sec, and chamber pressure reached 550 psia at $t_0 + 2.124$ sec. Engine vibration in excess of 150 g occurred for 33 msec beginning at $t_0 + 1.052$ sec. Gas generator outlet temperature first peak was 2020° F with no second peak.

4.2.13 Firing J4-1901-06D

The programmed 7.5-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 56. Start and shutdown transient operating times of selected engine valves are presented in Table VIII. Engine start and shutdown transients are shown in Fig. 57. Fuel pump start transient performance is shown in Fig. 58. Pressure altitude at engine start was 103,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 59.

Test conditions were selected to simulate an S-IVB 80-min restart with minimum start tank temperature and coldest thrust chamber. Augmented spark igniter ignition was detected 0.212 sec after engine start. Thrust chamber ignition occurred at $t_0 + 0.972$ sec, and chamber pressure reached 550 psia at $t_0 + 2.090$ sec. Engine vibration in excess of 150 g occurred for 25 msec beginning at $t_0 + 0.960$ sec. Gas generator outlet temperature first peak was 1930° F with no second peak.

4.2.14 Firing J4-1901-06E

The programmed 1.25-sec duration firing was successfully accomplished. Test conditions at engine start are presented in Table VI. Thermal conditioning histories of various engine components are shown in Fig. 60. Start and shutdown transient operating times of selected engine valves are presented in Table VII. Engine start and shutdown transients are shown in Fig. 61. Fuel pump start transient performance is shown in Fig. 62. Pressure altitude at engine start was 110,000 ft. Engine ambient and combustion chamber pressure histories are shown in Fig. 63.

Test conditions were selected to permit a determination of the effect of a -200°F oxidizer injector dome on start transient combustion stability with start conditions similar to firing 06A. Augmented spark igniter ignition was detected 0.237 sec after engine start, and thrust chamber ignition occurred at $t_0 + 1.093$ sec. Total duration of engine vibration in excess of 150 g was less than 10 msec before cutoff command. Gas generator outlet temperature first peak was $1840^{\circ}F$ with no second peak.

4.3 POST-TEST INSPECTION

The augmented spark igniter assembly was replaced following test 05 because of excessive seal leakage at the augmented spark igniter-to-injector interface. No other engine component damage was incurred during test periods J4-1901-03 through J4-1901-06.

SECTION V SUMMARY OF RESULTS

The results of testing the J-2 rocket engine in Test Cell J-4 during test periods J4-1901-03 through J4-1901-06 between July 23 and August 15, 1968, are summarized as follows:

- 1. All primary objectives were satisfactorily accomplished.
- 2. Augmented spark igniter ignition was not detected before mainstage signal under conditions simulating an S-II start at minimum augmented spark igniter mixture ratio.
- 3. An oxidizer injector dome temperature of -200°F had no detectable effect on start transient combustion stability.
- 4. Except for a leaking seal at the augmented spark igniter-to-injector interface, no engine component damage was incurred.

REFERENCES

- 1. Dubin, M., Sissenwine, N., and Wexler, H. <u>U.S. Standard</u> Atmosphere, 1962. December 1962.
- 2. Counts, H. J., Jr., and Kunz, C. H. "Altitude Developmental and Flight Support Testing of the J-2 Rocket Engine in Propulsion Engine Test Cell (J-4) (Tests J4-1801-42 through J4-1901-02)." AEDC-TR-68-223, November 1968.
- 3. "J-2 Rocket Engine, Technical Manual Engine Data." R-3825-1, August 1965.
- 4. Test Facilities Handbook (7th Edition). "Large Rocket Facility,
 Vol. 3." Arnold Engineering Development Center, July 1968.

APPENDIXES

- I. ILLUSTRATIONS
- II. TABLES
- III. INSTRUMENTATION
- IV. METHOD OF CALCULATION (PERFORMANCE PROGRAM)

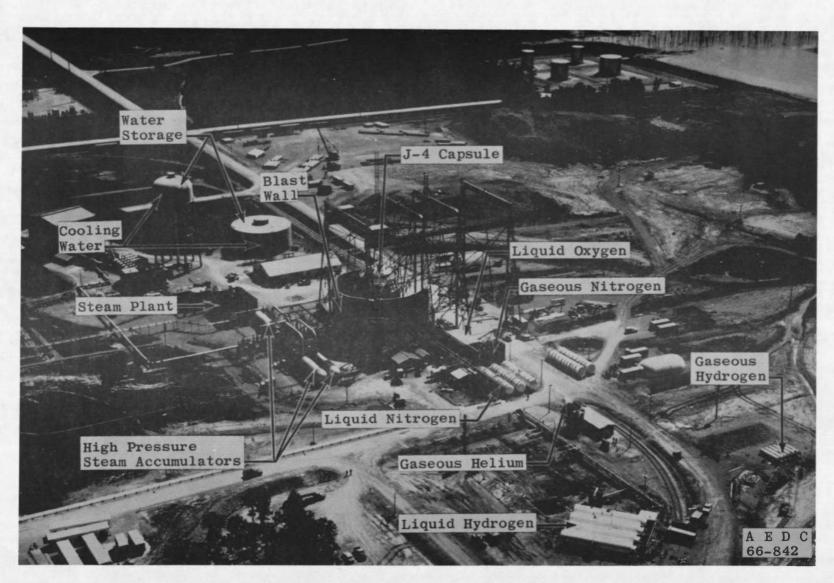


Fig. 1 Test Cell J-4 Complex

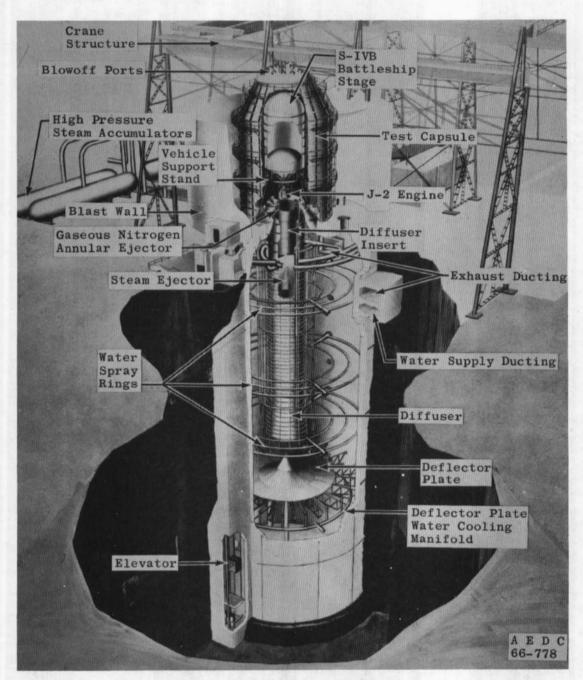


Fig. 2 Test Cell J-4, Artist's Conception

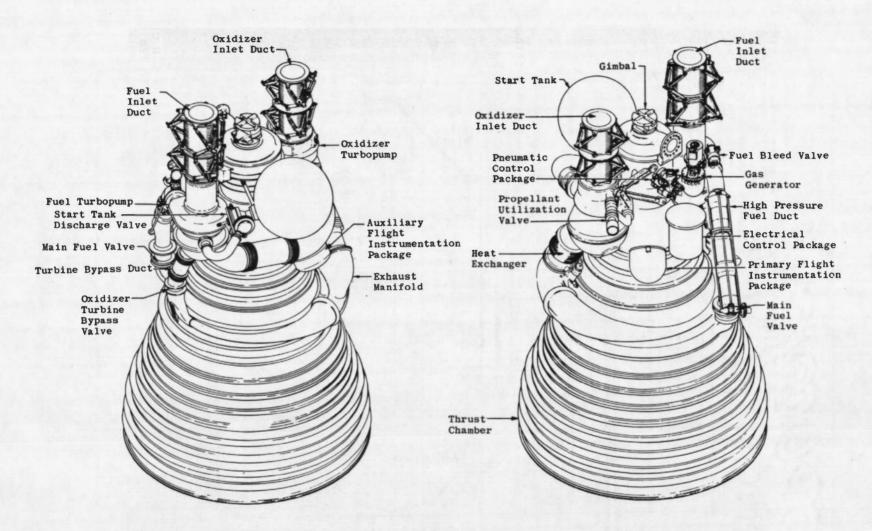


Fig. 3 Engine Details

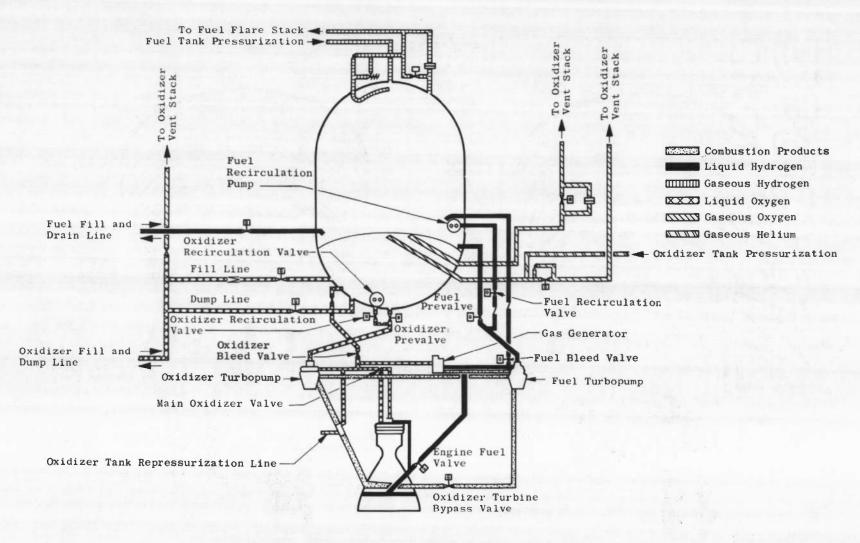
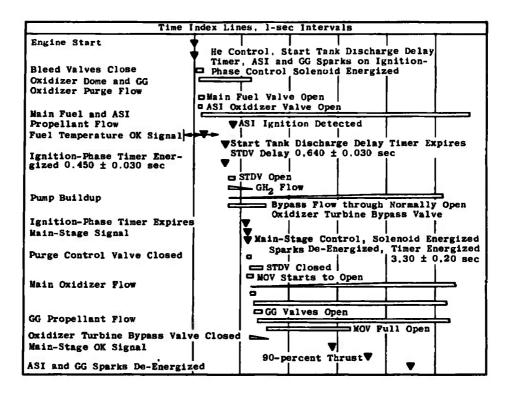
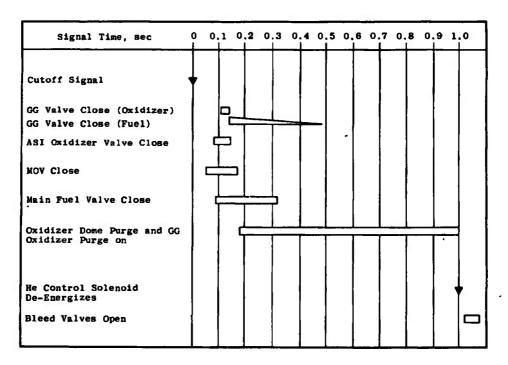


Fig. 4 S-IVB Battleship Stage /J-2 Engine Schematic

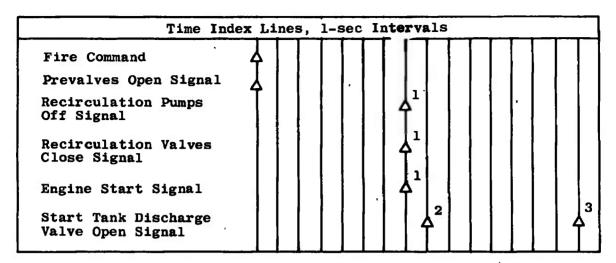


a. Start Sequence



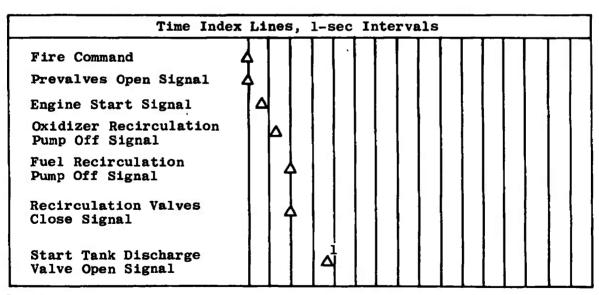
b. Shutdown Sequence

Fig. 7 Engine Start and Shutdown Sequence



¹ Nominal Occurrence Time (Function of Prevalves Opening Time)

c. "Normal" Start Sequence



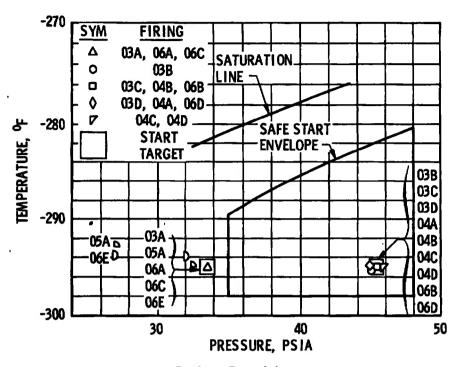
¹ Three-sec Fuel Lead (S-IVB/S-V First Burn)

d. "Auxiliary" Start Sequence

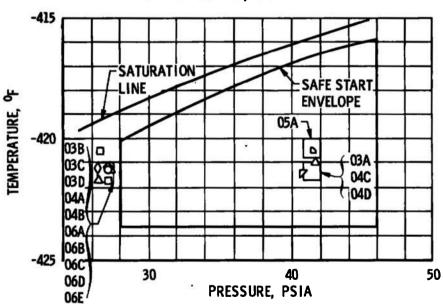
Fig. 7 Concluded

 $^{^2}$ One-sec Fuel Lead (S-II/S-V and S-IVB/S-IB)

³Eight-sec Fuel Lead (S-IVB/S-V and S-IB Orbital Restart)

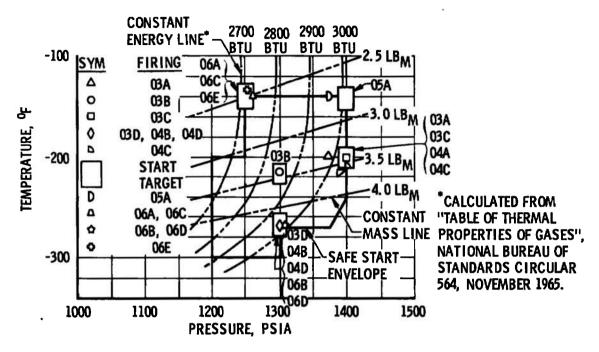




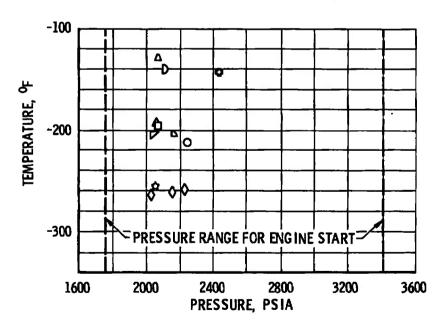


b. Fuel Pump Inlet

Fig. 8 Engine Start Conditions for the Pump Inlets, Start Tank, and Helium Tank



c. Start Tank



d. Helium Tank

Fig. 8 Concluded

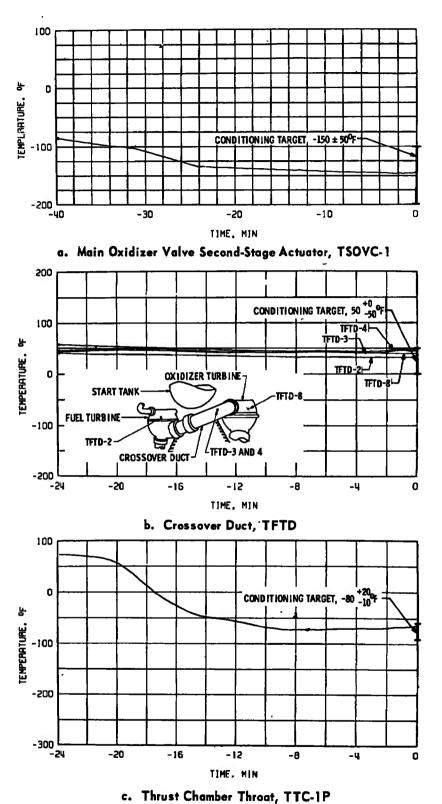
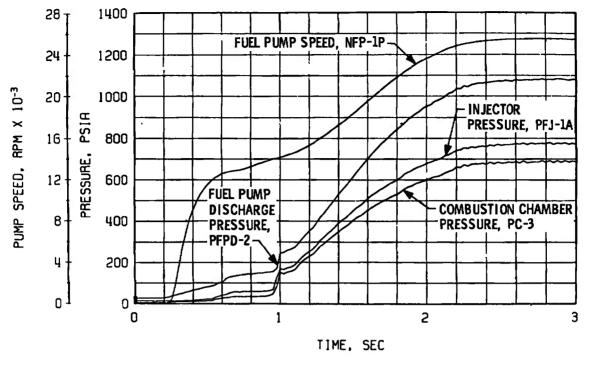


Fig. 9 Thermal Conditioning History of Engine Components, Firing 03A



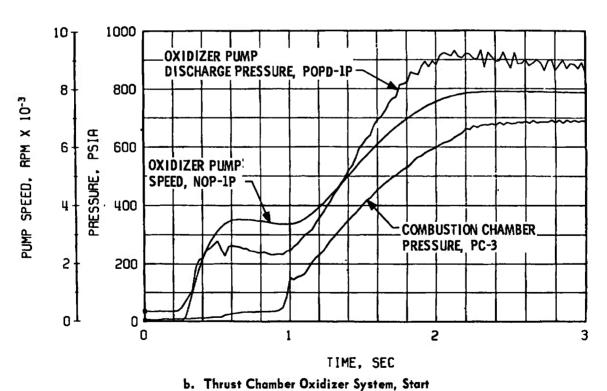
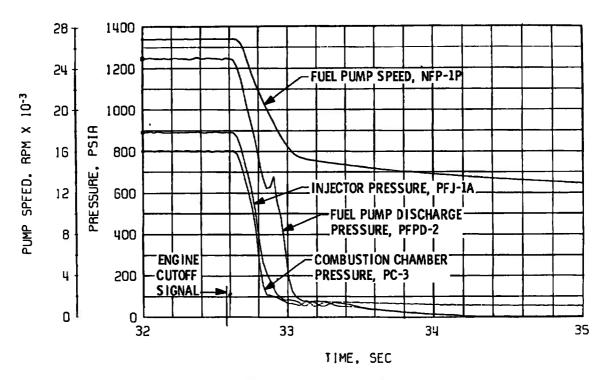
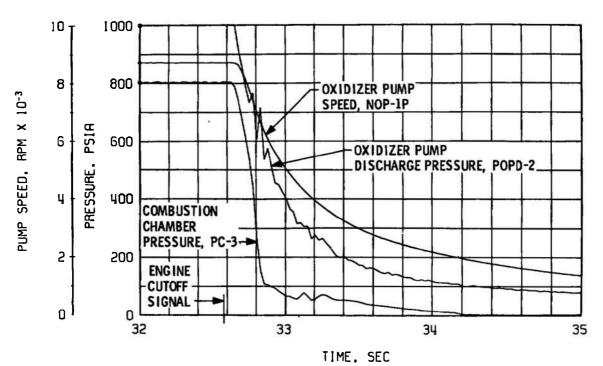


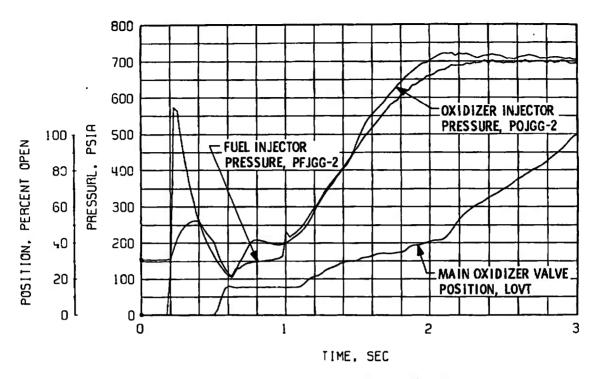
Fig. 10 Engine Transient Operation, Firing 03A



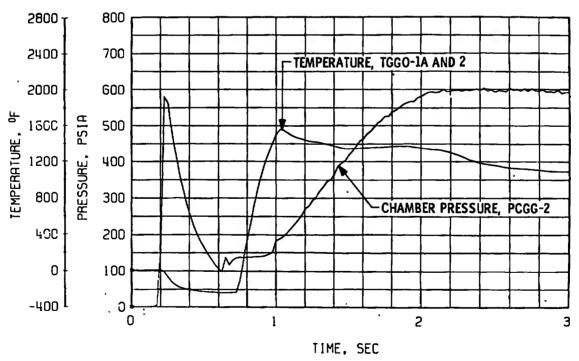
c. Thrust Chamber Fuel System, Shutdown



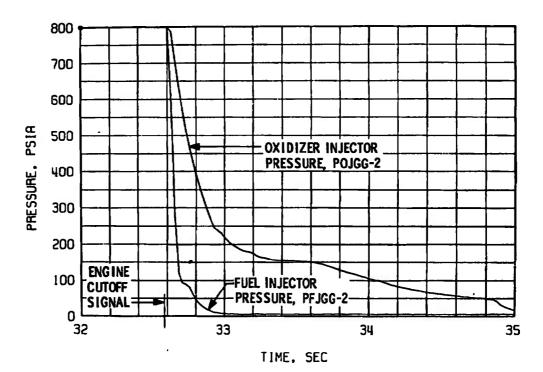
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 10 Continued



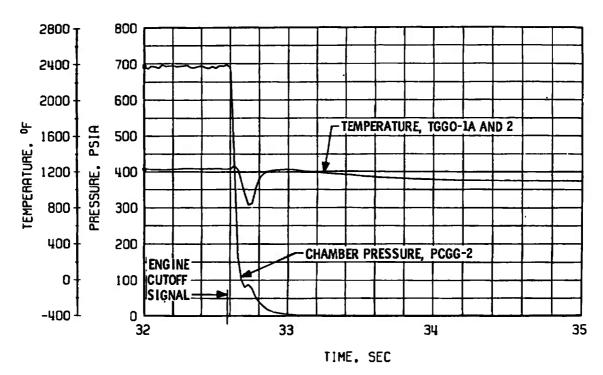
e. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start Fig. 10 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown Fig. 10 Concluded

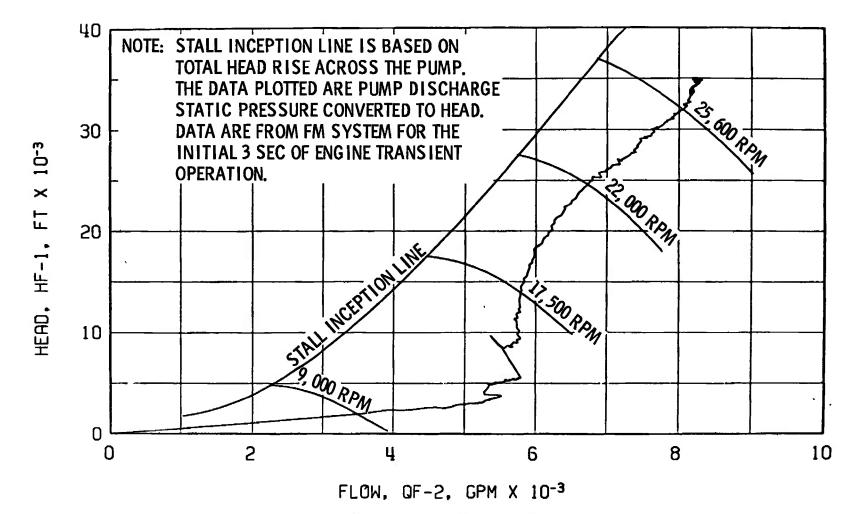


Fig. 11 Fuel Pump Start Transient Performance, Firing 03A

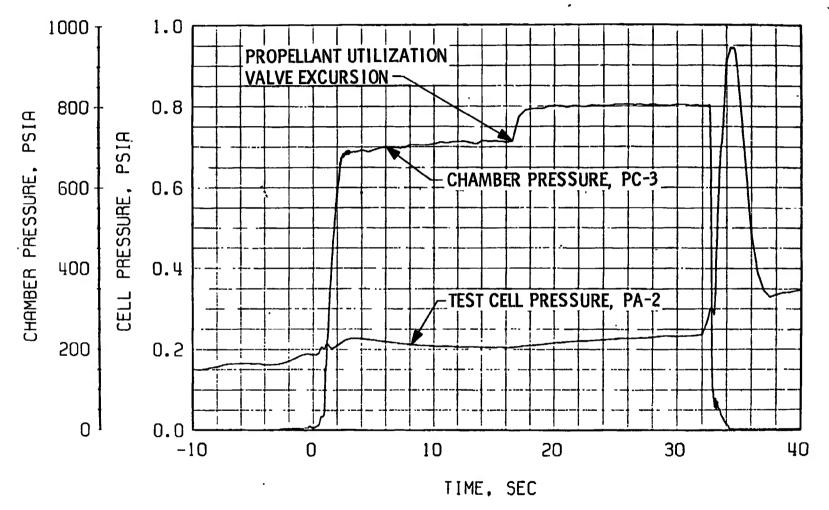
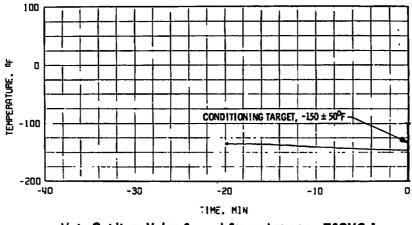
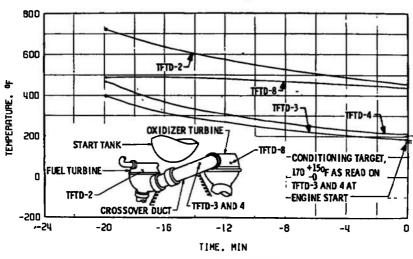
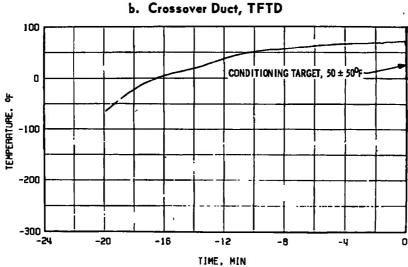


Fig. 12 Engine Ambient and Combustion Chamber Pressure, Firing 03A



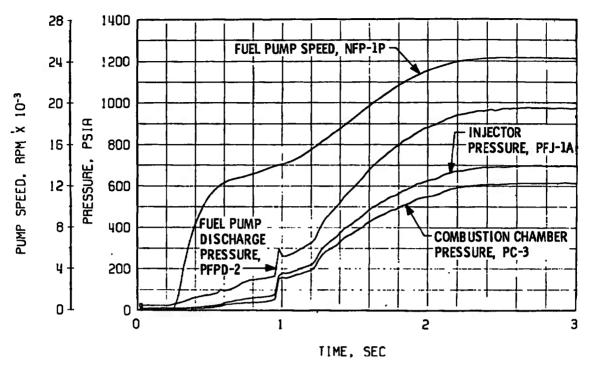
a. Moin Oxidizer Valve Second-Stage Actuator, TSOVC-1

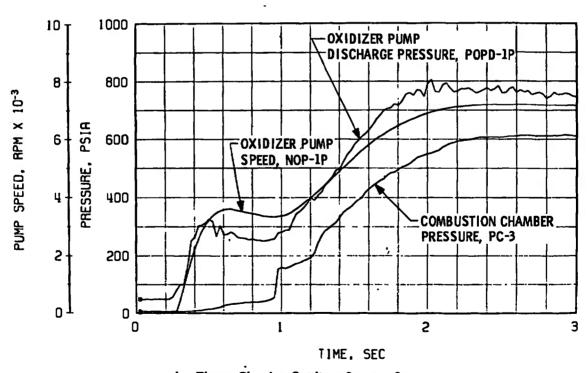




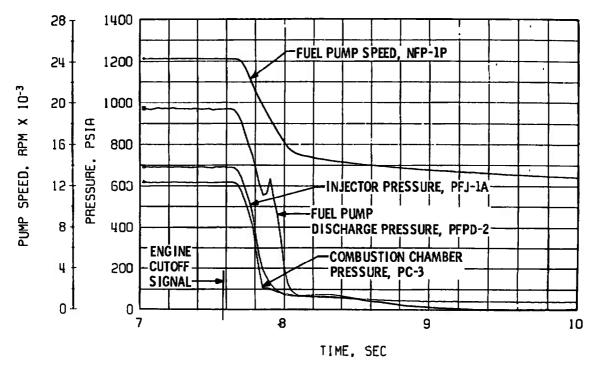
c. Thrust Chamber Throat, TTC-1P

Fig. 13 Thermal Conditioning History of Engine Components, Firing 03B

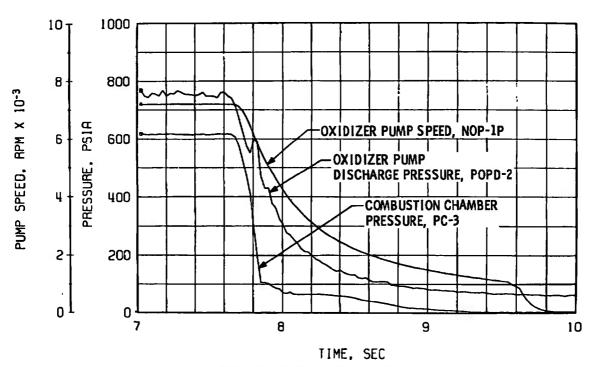




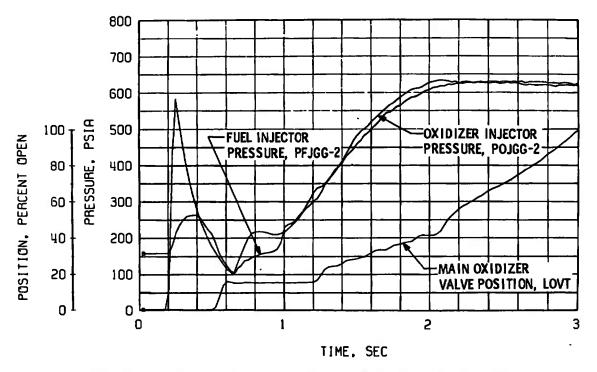
b. Thrust Chamber Oxidizer System, StartFig. 14 Engine Transient Operation, Firing 03B



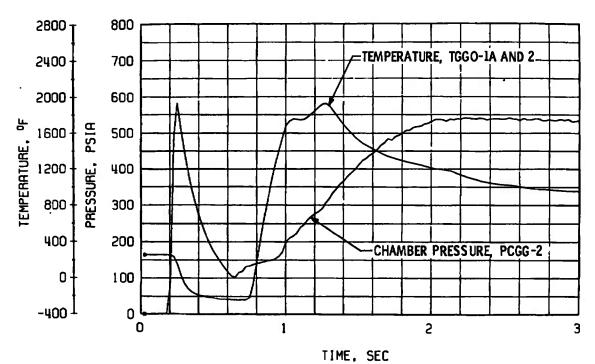
c. Thrust Chamber Fuel System, Shutdown



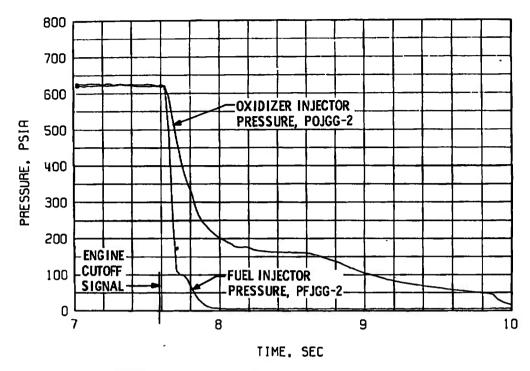
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 14 Continued



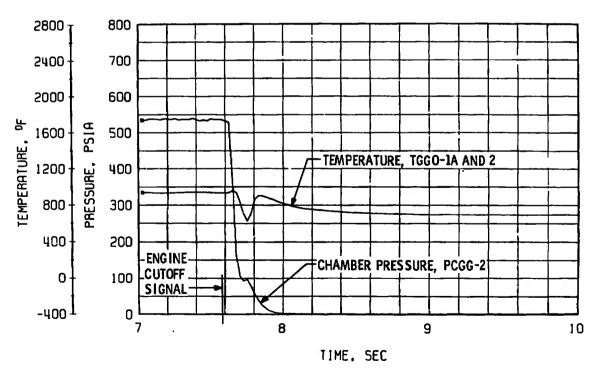
e. Gas Generator Injectar Pressures and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start Fig. 14 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdawn
Fig. 14 Concluded



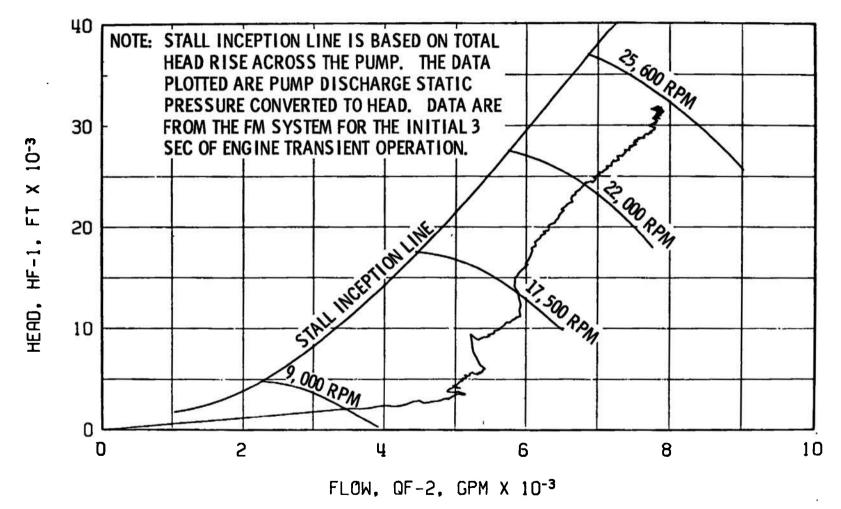


Fig. 15 Fuel Pump Start Transient Performance, Firing 03B

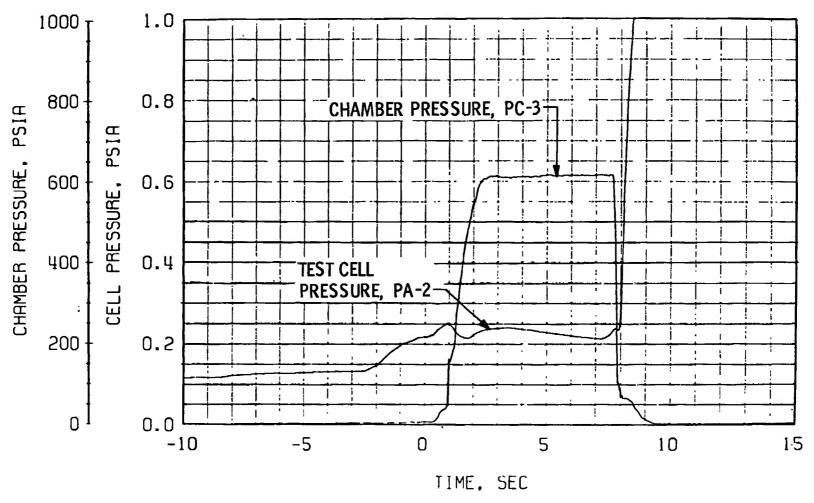


Fig. 16 Engine Ambient and Combustion Chamber Pressure, Firing 03B

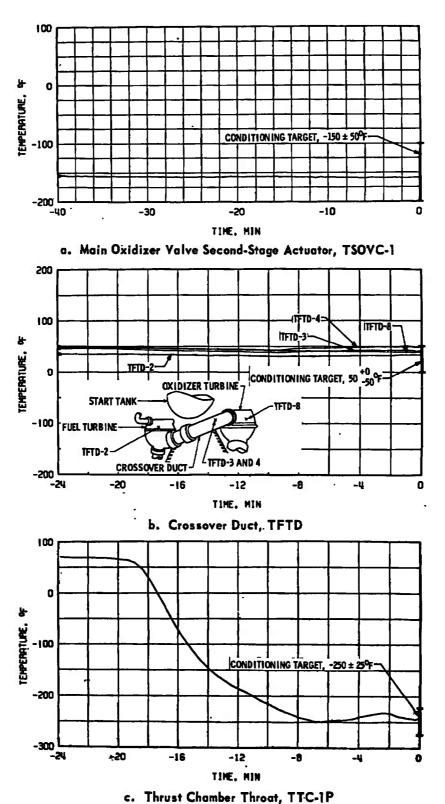
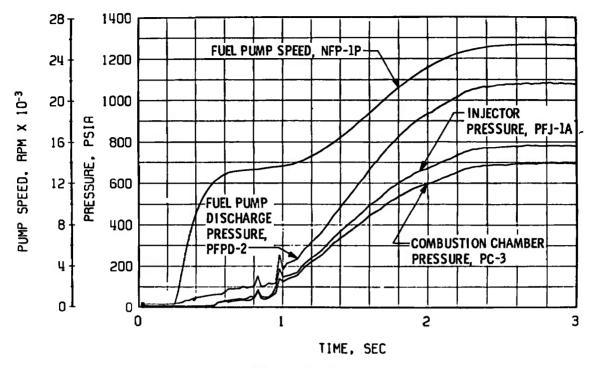
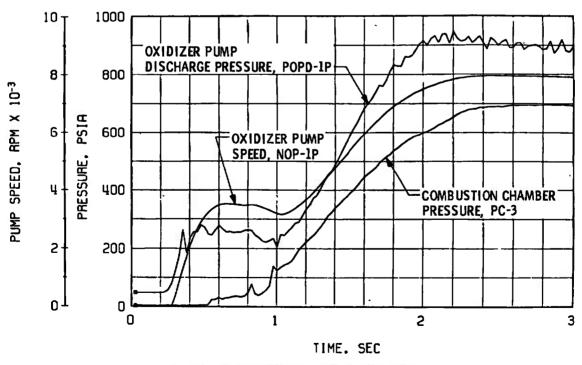


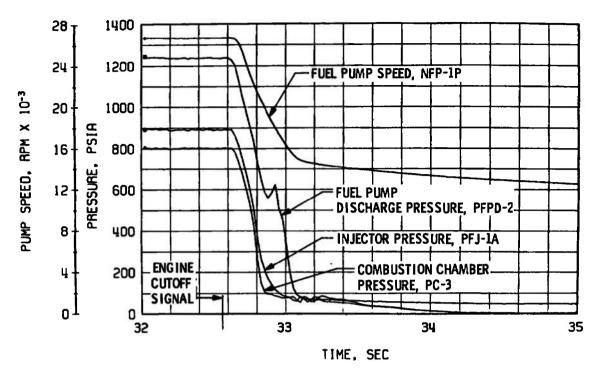
Fig. 17 Thermal Conditioning History of Engine Components, Firing 03C



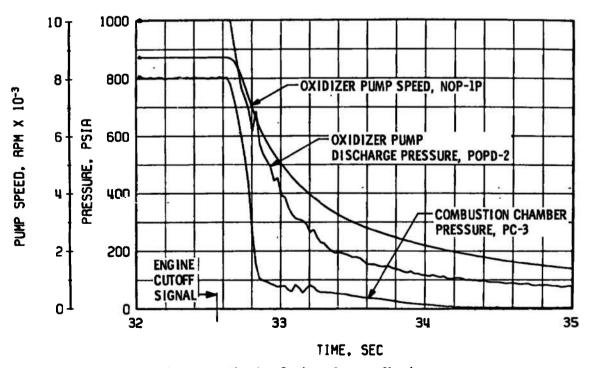




b. Thrust Chamber Oxidizer System, Start .
Fig. 18 Engine Transient Operation, Firing 03C

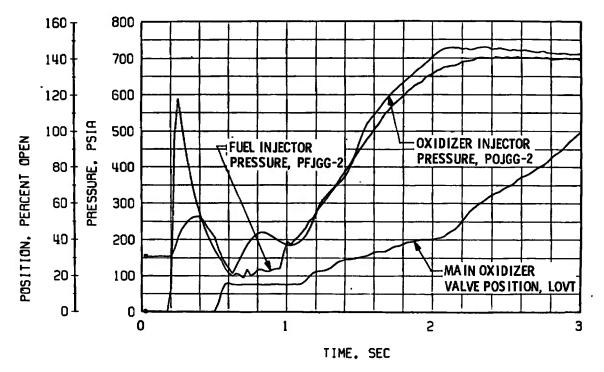


c. Thrust Chamber Fuel System, Shutdown

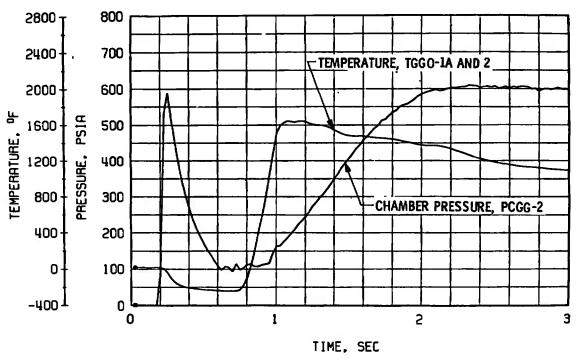


d. Thrust Chamber Oxidizer System, Shutdown

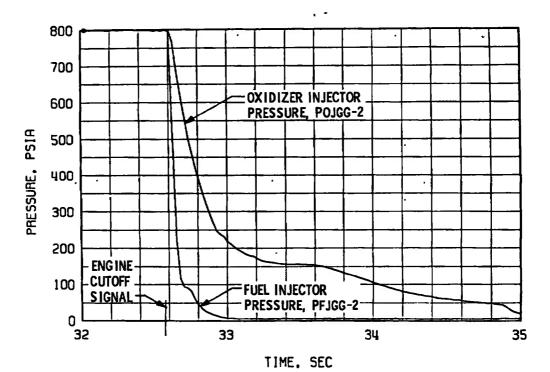
Fig. 18 Continued



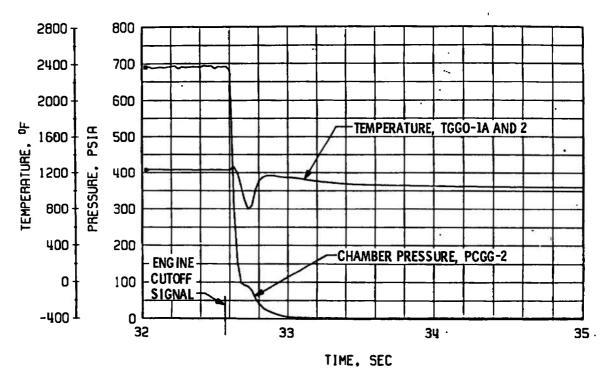
e. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start
Fig. 18 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown
Fig. 18 Concluded

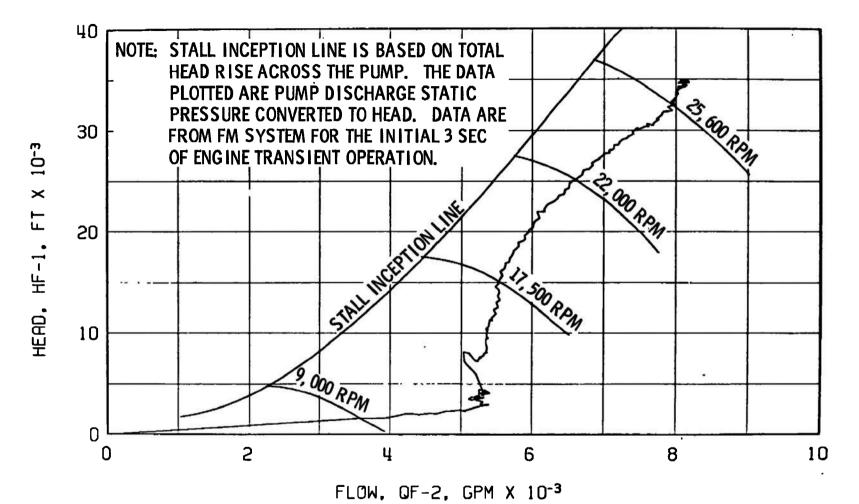


Fig. 19 Fuel Pump Start Transient Performance, Firing 03C



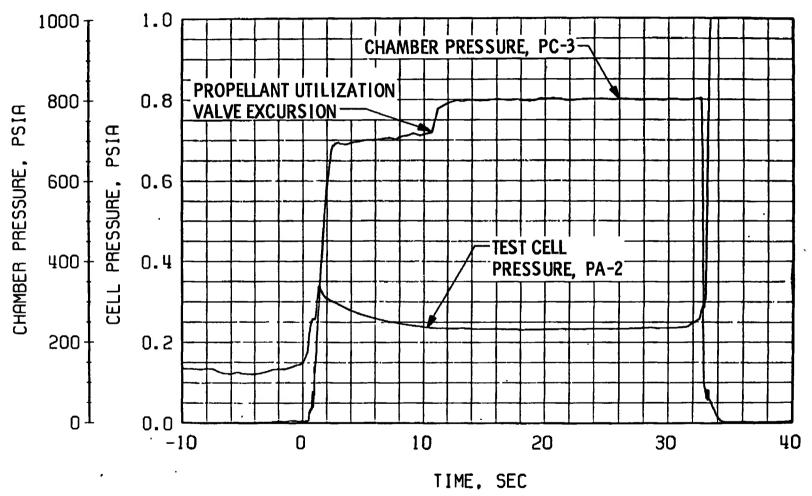
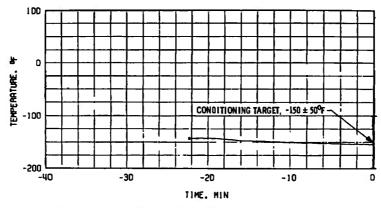
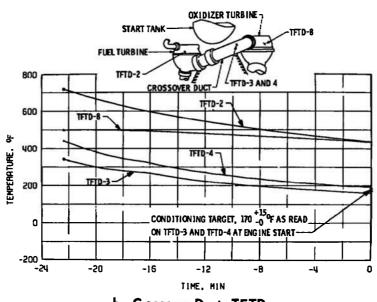
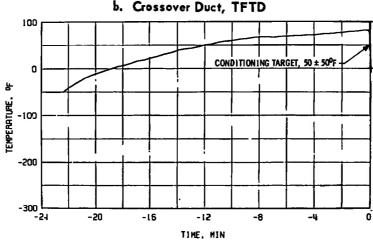


Fig. 20 Engine Ambient and Combustion Chamber Pressure, Firing 03C



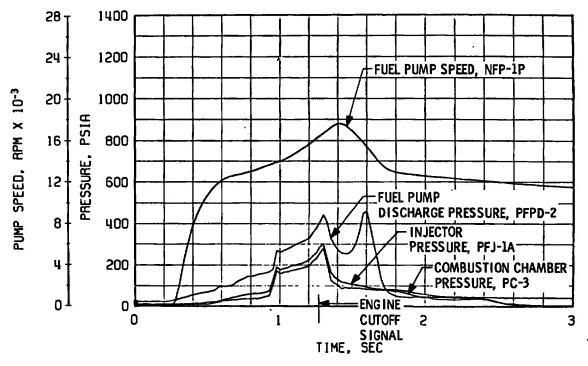
a. Main Oxidizer Valve Second-Stage Actuator, TSOVC-1



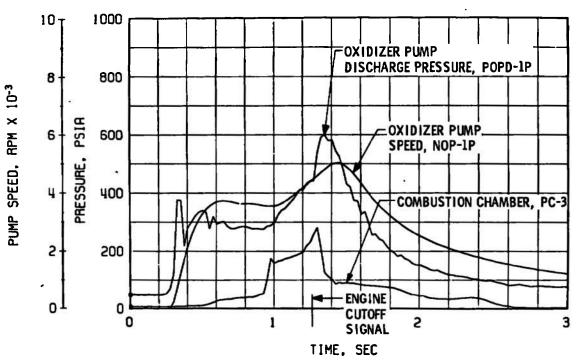


c. Thrust Chamber Throat, TTC-1P

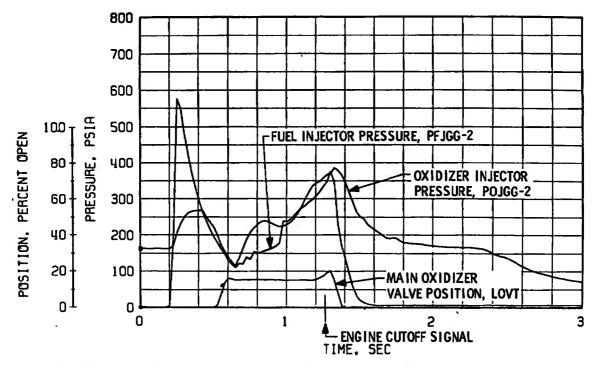
Fig. 21 Thermal Conditioning History of Engine Components, Firing 03D



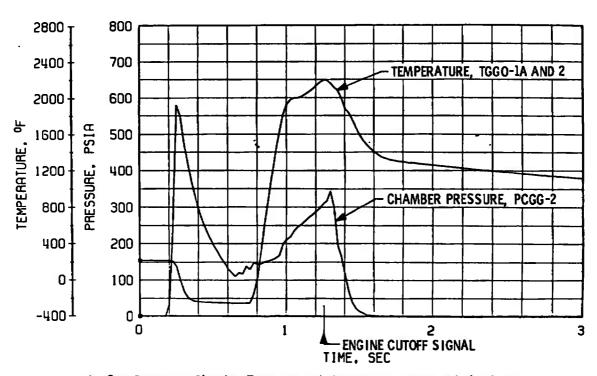
a. Thrust Chamber Fuel System, Start and Shutdown



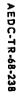
Thrust Chamber Oxidizer System, Start and Shutdown
 Fig. 22 Engine Transient Operation, Firing 03D



c. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start and Shutdown



d. Gas Generator Chamber Pressure and Temperature, Start and Shutdown
Fig. 22 Concluded



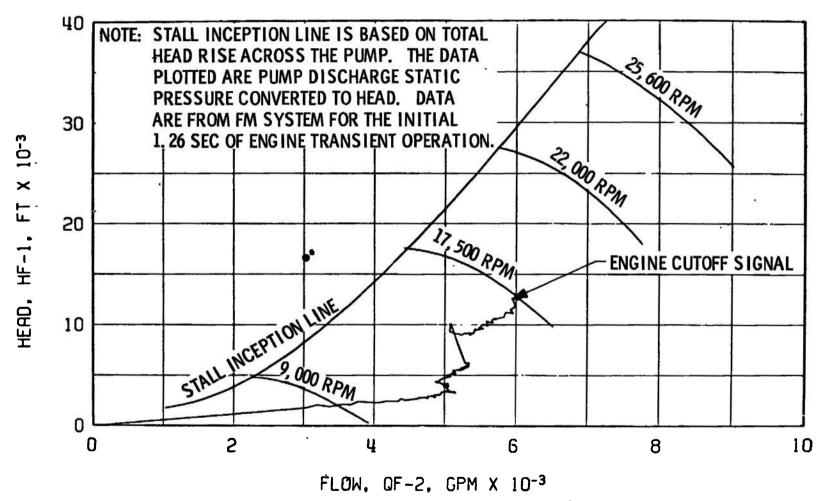


Fig. 23 Fuel Pump Start Transient Performance, Firing 03D

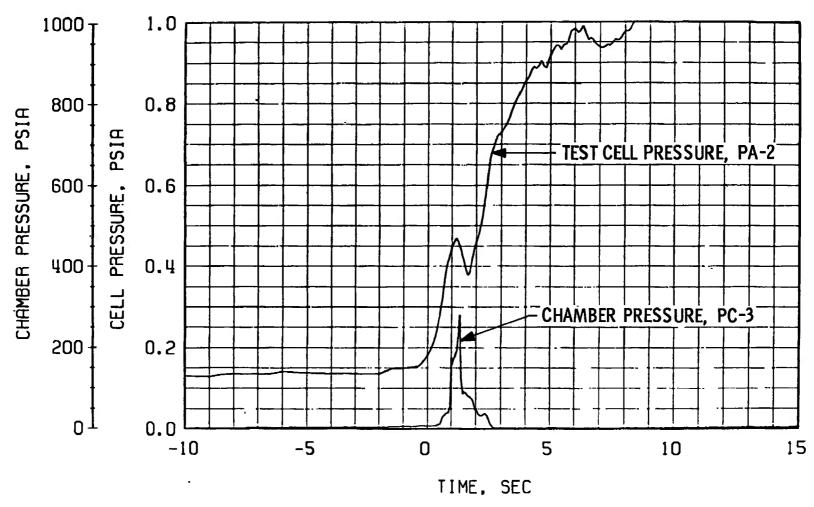


Fig. 24 Engine Ambient and Combustion Chamber Pressure, Firing 03D

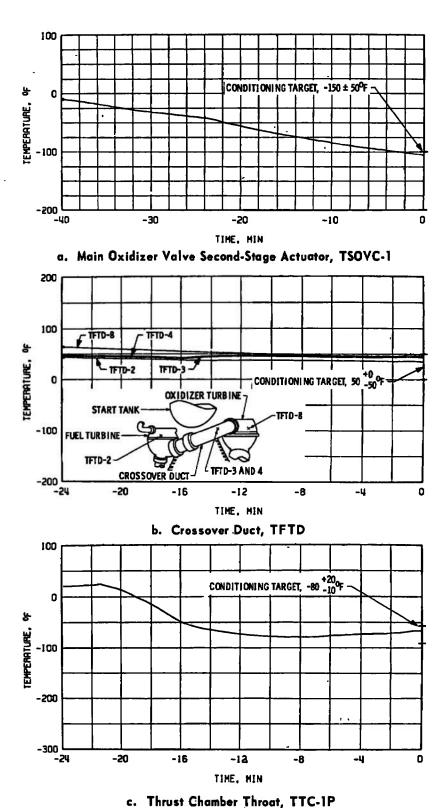
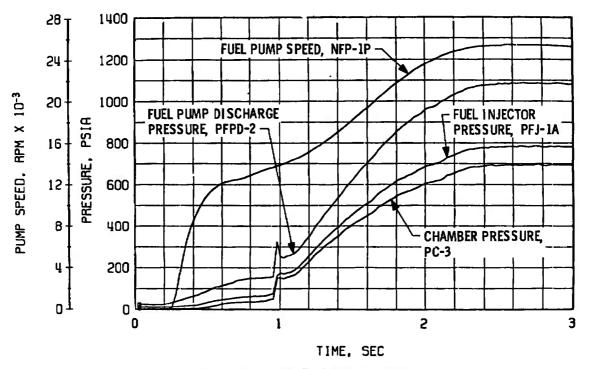
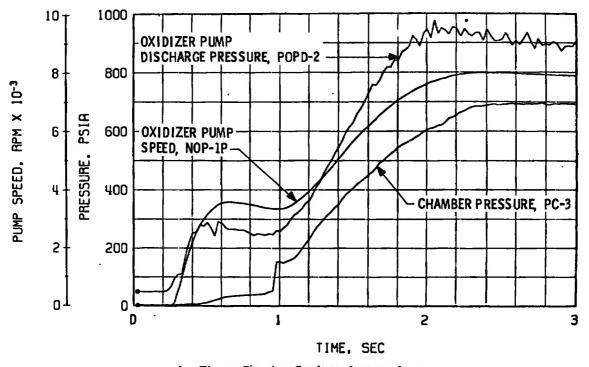
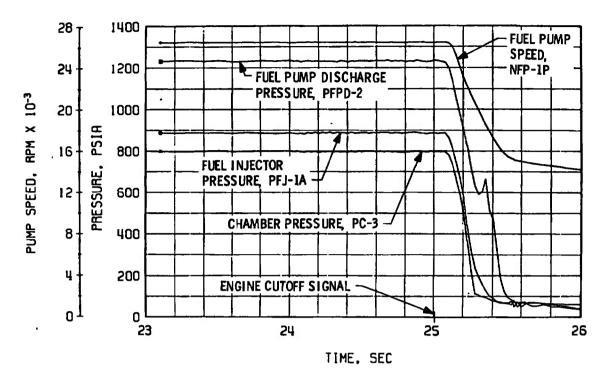


Fig. 25 Thermal Conditioning History of Engine Components, Firing 04A

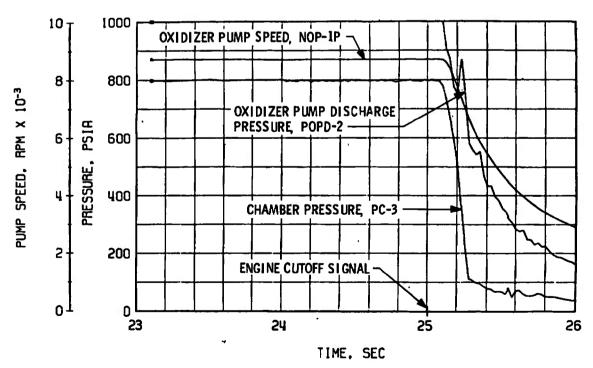




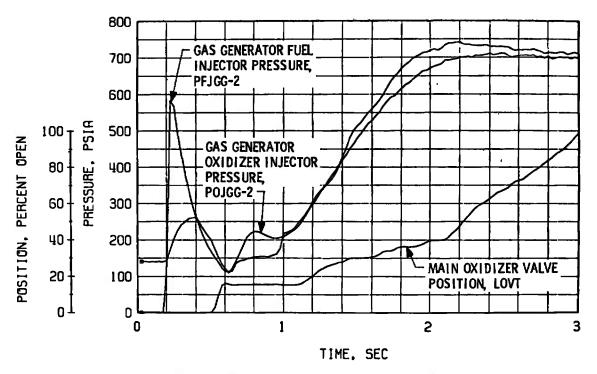
b. Thrust Chamber Oxidizer System, Start
Fig. 26 Engine Transient Operation, Firing Ü4A



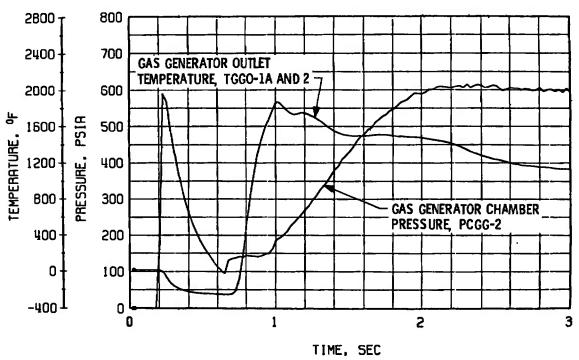
c. Thrust Chamber Fuel System, Shutdown



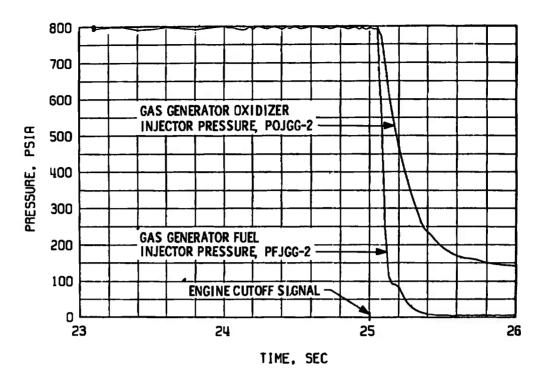
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 26 Continued



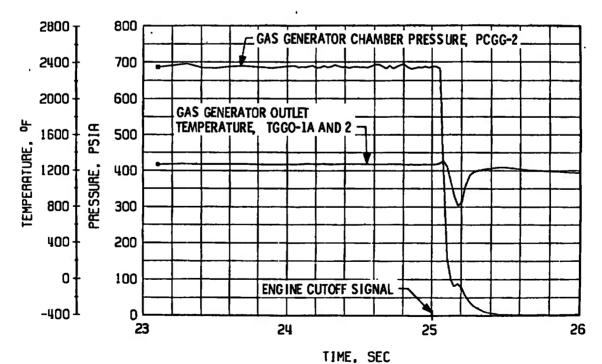
e. Gas Generator Injector Pressure and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start Fig. 26 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown Fig. 26 Concluded

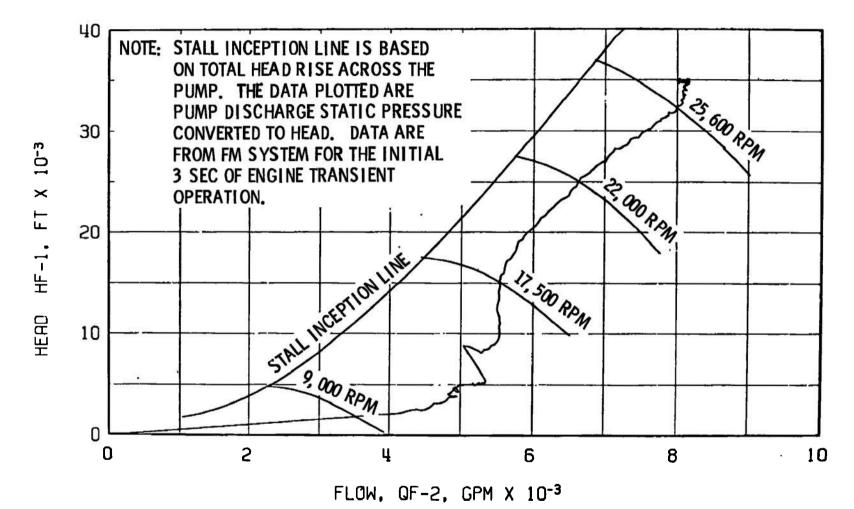


Fig. 27 Fuel Pump Start Transient Performance, Firing 04A

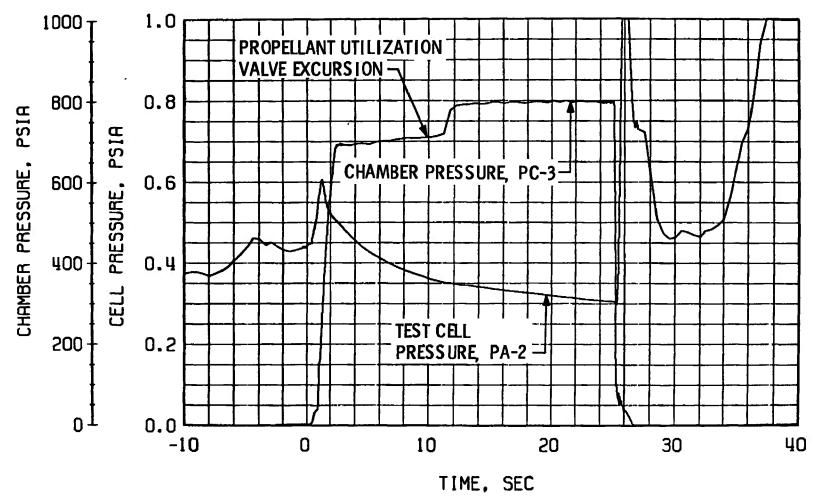
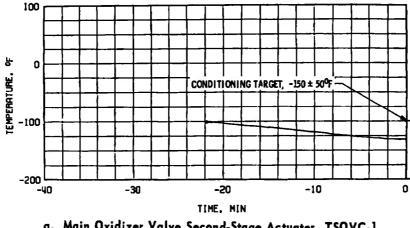
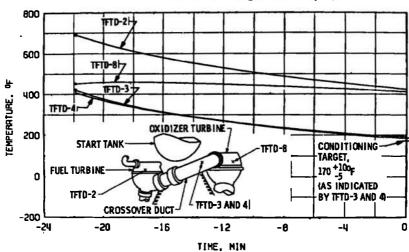


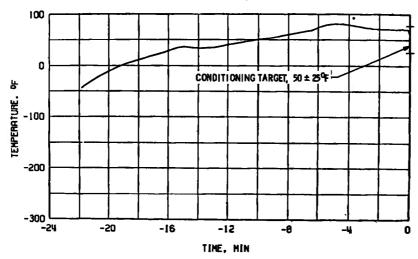
Fig. 28 Engine Ambient and Combustion Chamber Pressure, Firing 04A



a. Main Oxidizer Valve Second-Stage Actuator, TSOVC-1

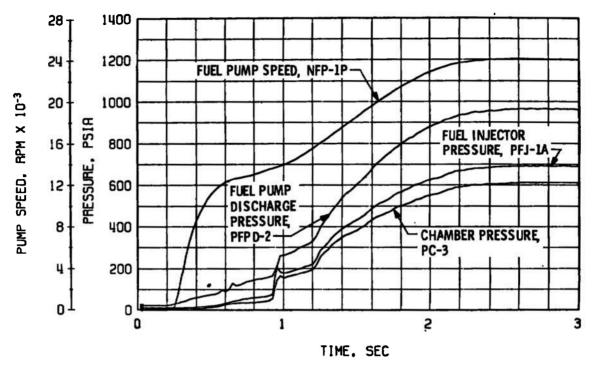


b. Crossover Duct, TFTD



c. Thrust Chamber Throat, TTC-1P

Fig. 29 Thermal Conditioning History of Engine Components, Firing 04B



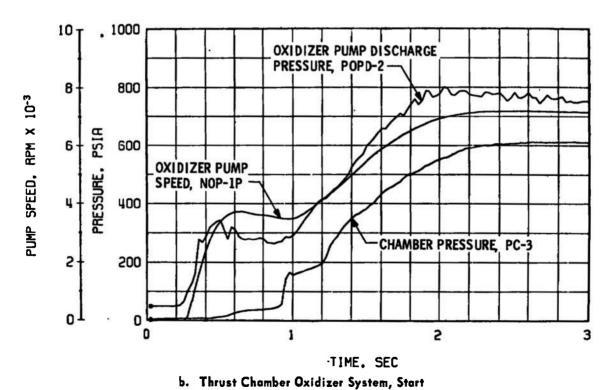
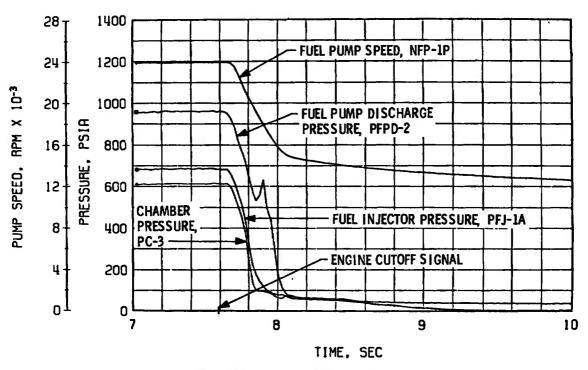
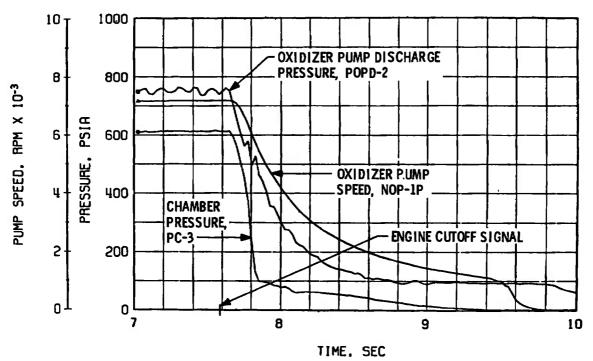


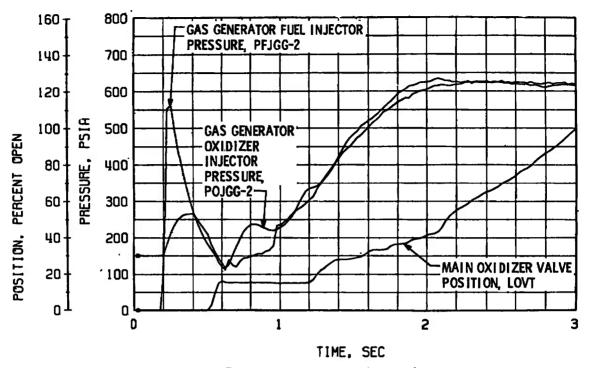
Fig. 30 Engine Transient Operation, Firing 04B



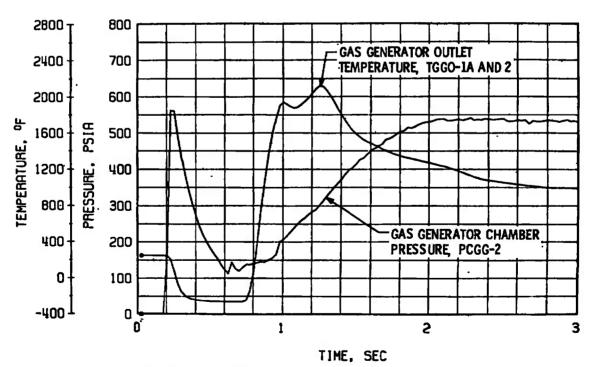
c. Thrust Chamber Fuel System, Shutdown



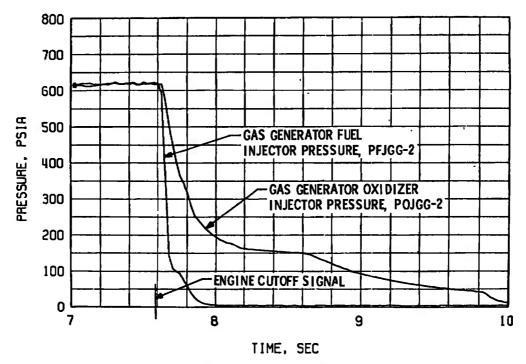
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 30 Continued



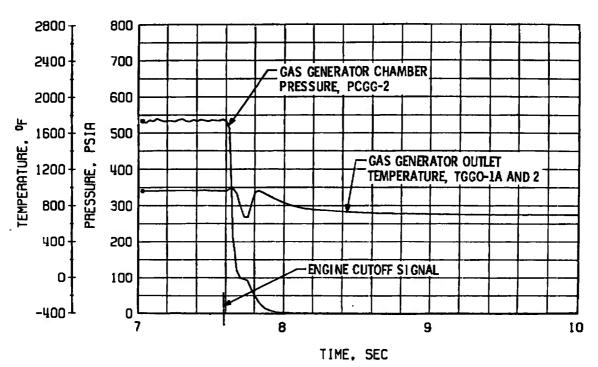
e. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start Fig. 30 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown
Fig. 30 Concluded



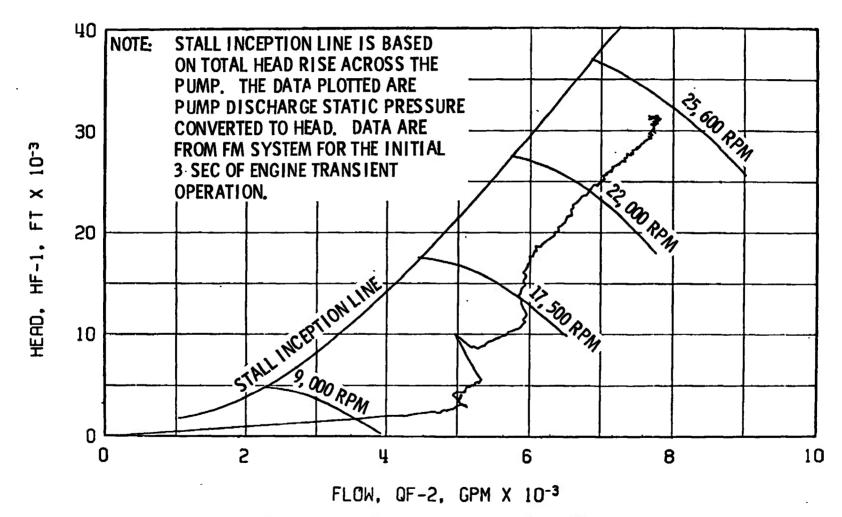


Fig. 31 Fuel Pump Start Transient Performance, Firing 04B

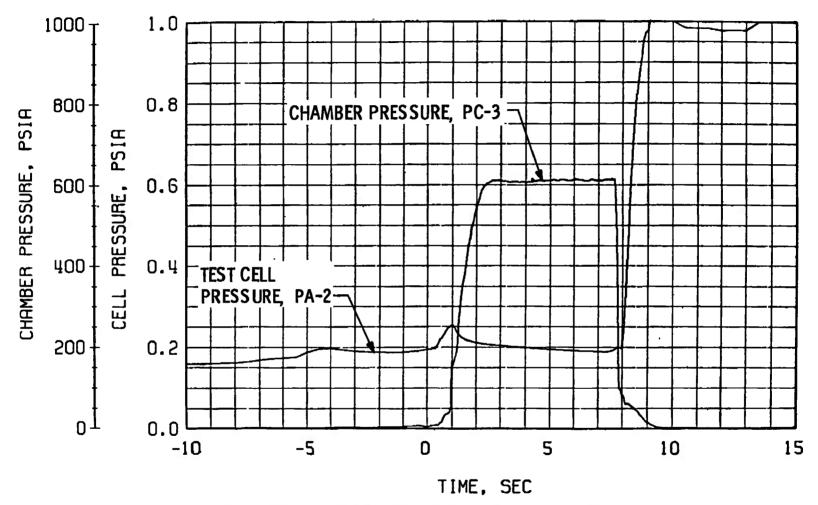


Fig. 32 Engine Ambient and Combustion Chamber Pressure, Firing 04B

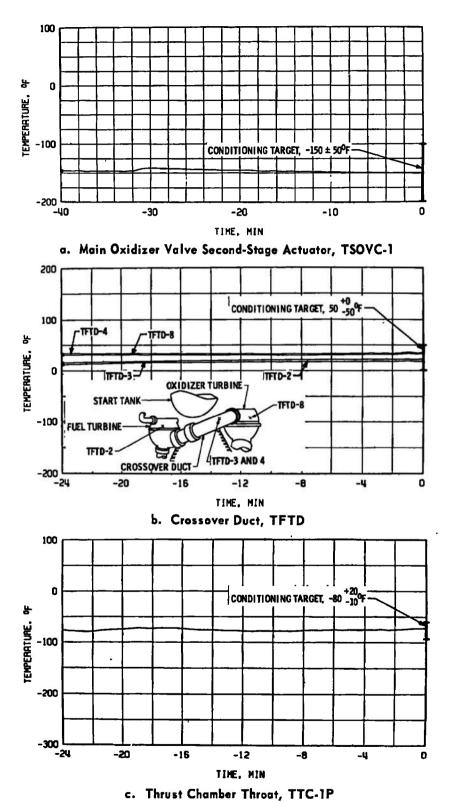
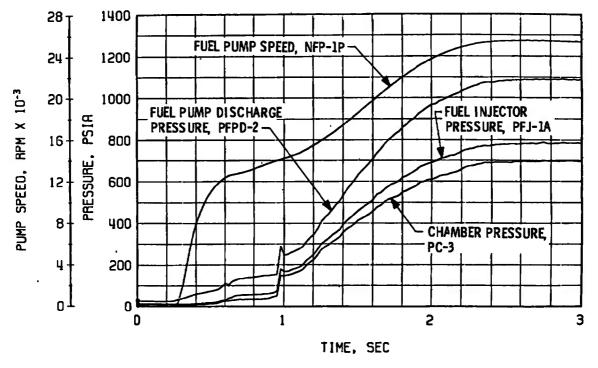
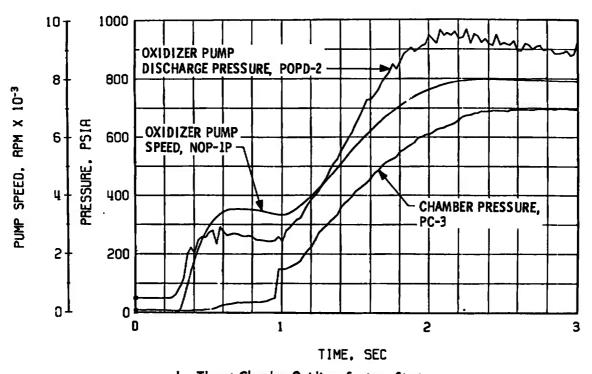


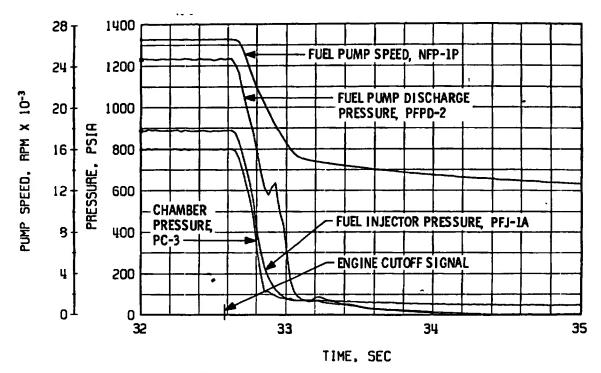
Fig. 33 Thermal Conditioning History of Engine Components, Firing 04C



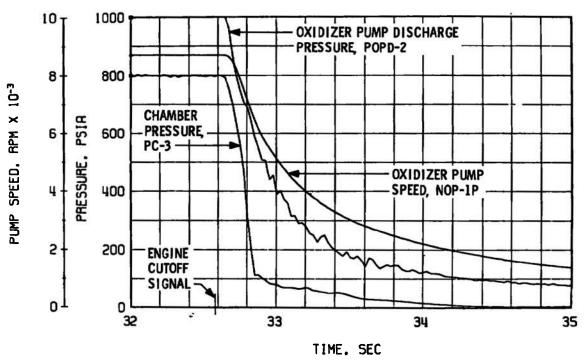
a. Thrust Chamber Fuel System, Start



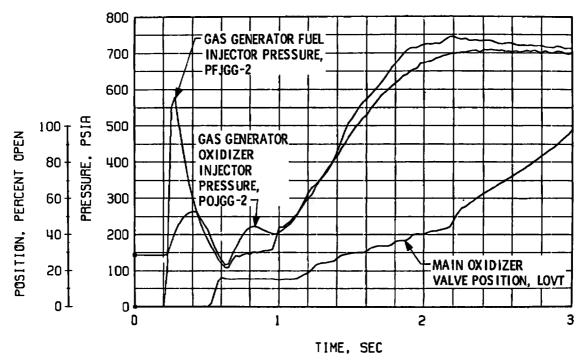
b. Thrust Chamber Oxidizer System, Start Fig. 34 Engine Transient Operation, Firing 04C



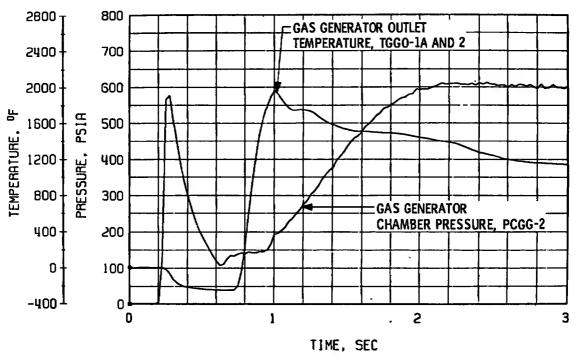
c. Thrust Chamber Fuel System, Shutdown



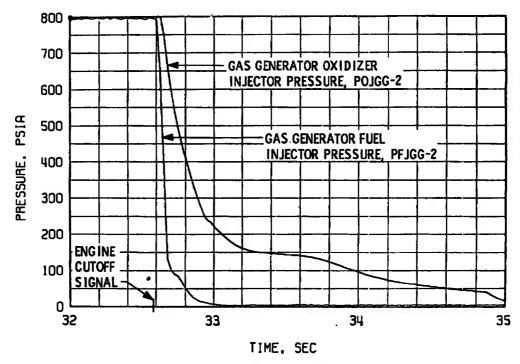
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 34 Continued



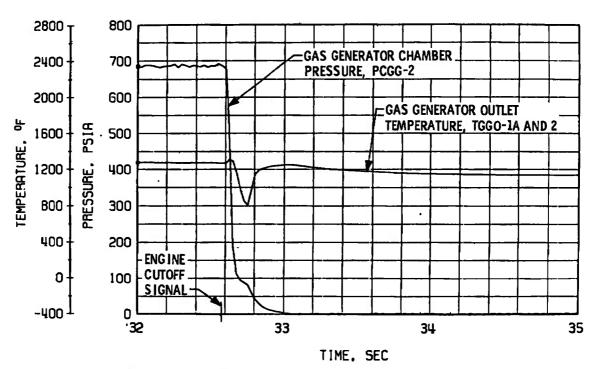
e. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Stort



f. Gas Generator Chamber Pressure and Temperature, Start Fig. 34 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown
Fig. 34. Concluded

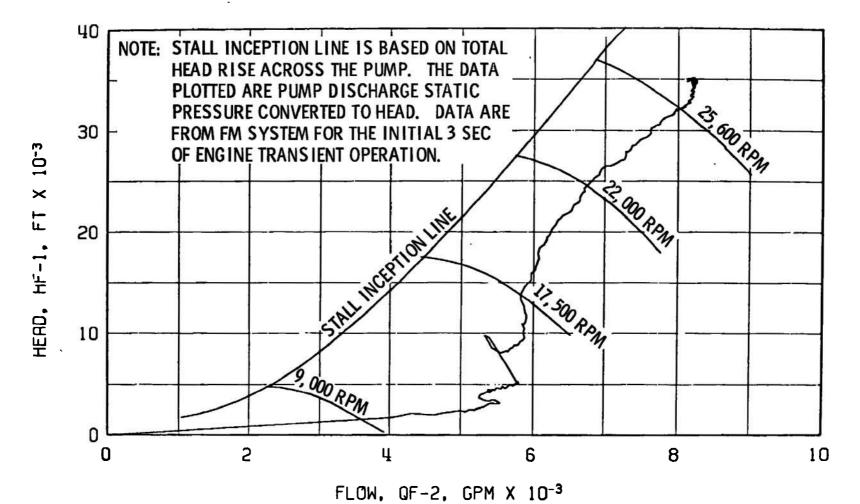


Fig. 35 Fuel Pump Start Transient Performance, Firing 04C



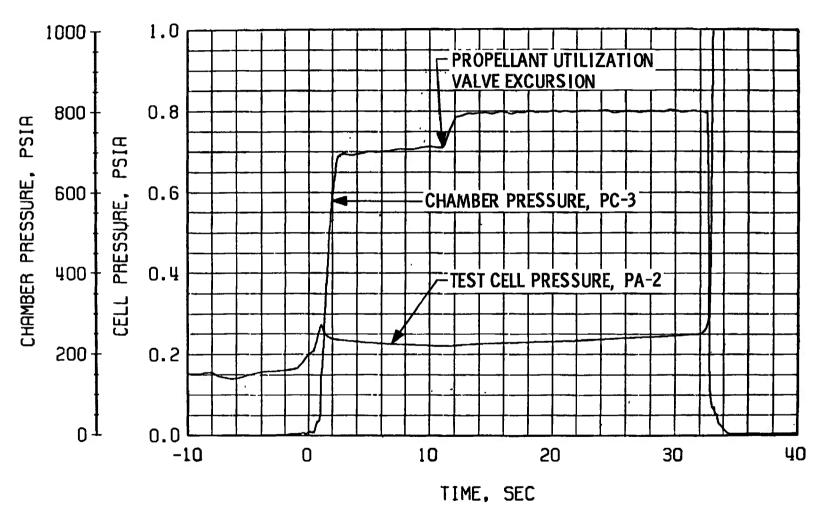


Fig. 36 Engine Ambient and Combustion Chamber Pressure, Firing 04C

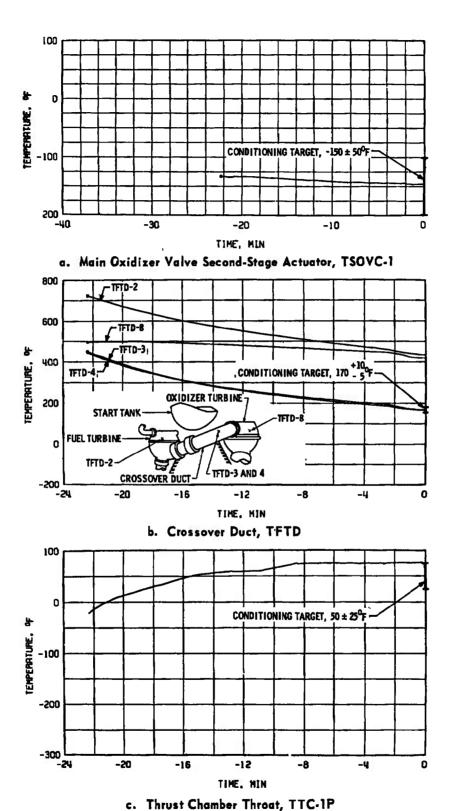
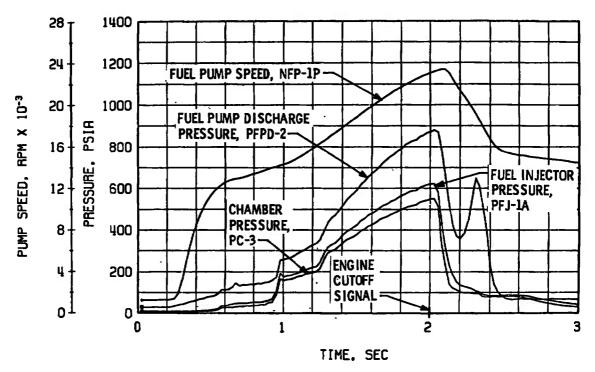
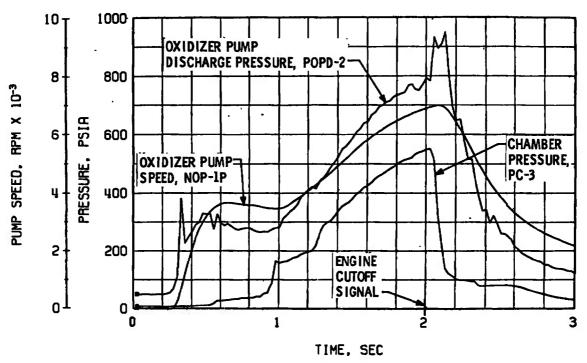


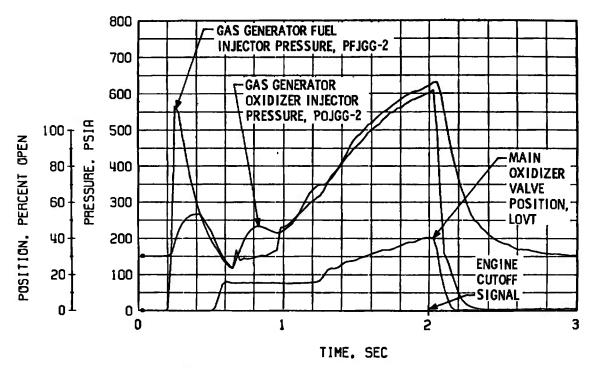
Fig. 37 Thermal Conditioning History of Engine Components, Firing 04D



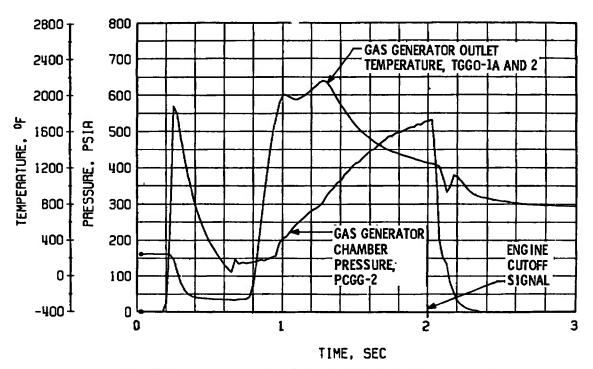
a. Thrust Chamber Fuel System, Start and Shutdown



Thrust Chamber Oxidizer System, Start and Shutdown
 Fig. 38 Engine Transient Operation, Firing 04D



c. Gas Generator Injectar Pressures and Main Oxidizer Valve Pasitian, Start and Shutdown



d. Gas Generatar Chamber Pressure and Temperature, Start and Shutdown Fig. 38 Concluded

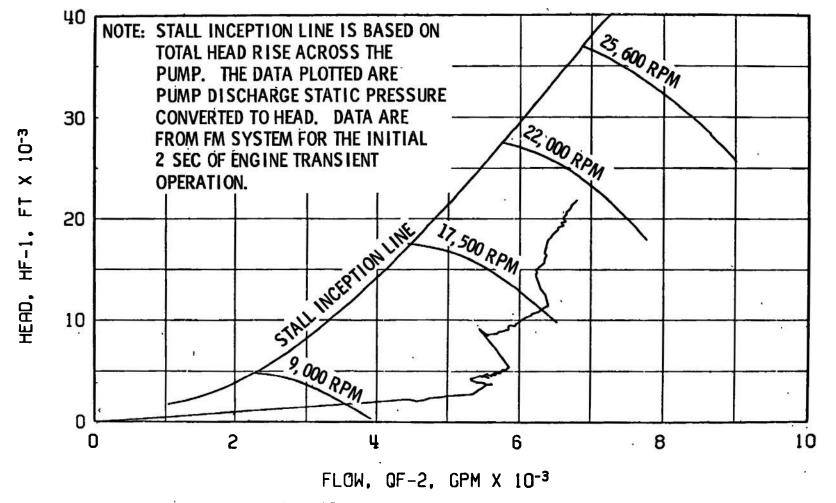


Fig. 39 Fuel Pump Start Transient Performance, Firing 04D

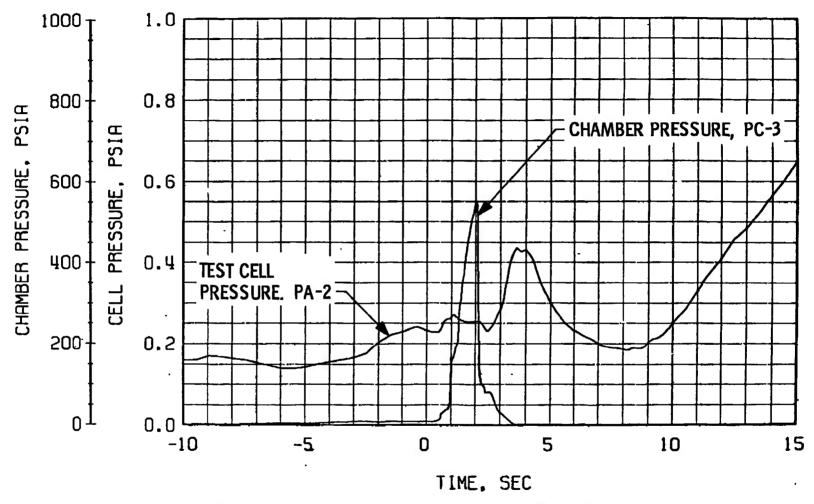
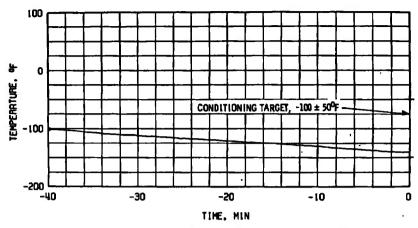
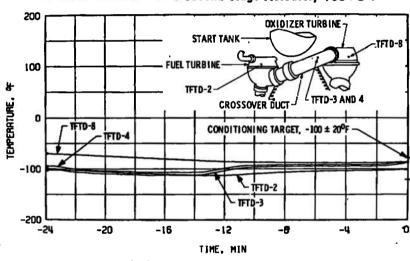


Fig. 40 Engine Ambient and Combustion Chamber Pressure, Firing 04D



a. Main Oxidizer Valve Second-Stage Actuator, TSOVC-1



B. Crossover Duct, TFTD

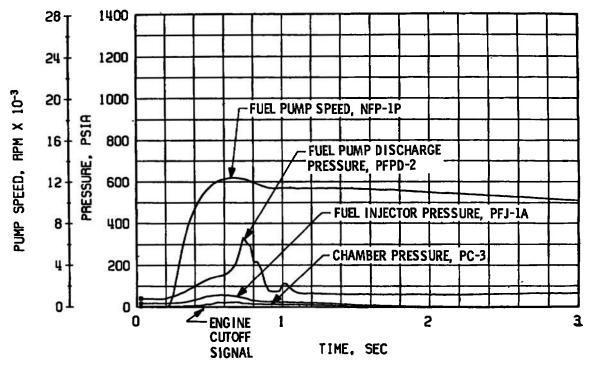
CONDITIONING TARGET, -150 +200 F

CONDITIONING TARGET, -150 -100 F

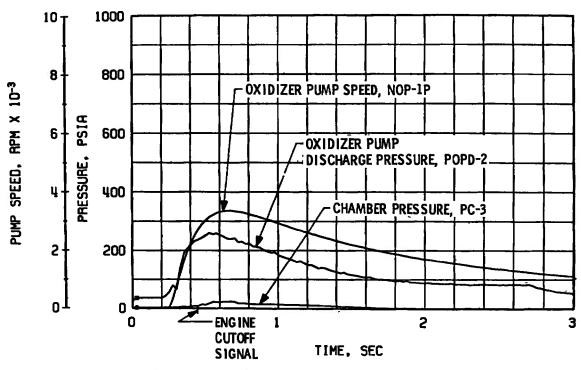
TIME, MIN

c. Thrust Chamber Throat, TTC-1P

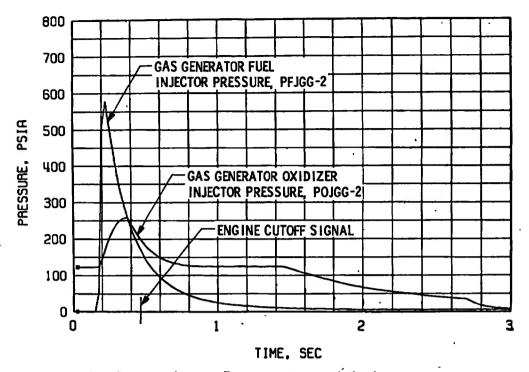
Fig. 41 Thermal Conditioning History of Engine Components, Firing 05A



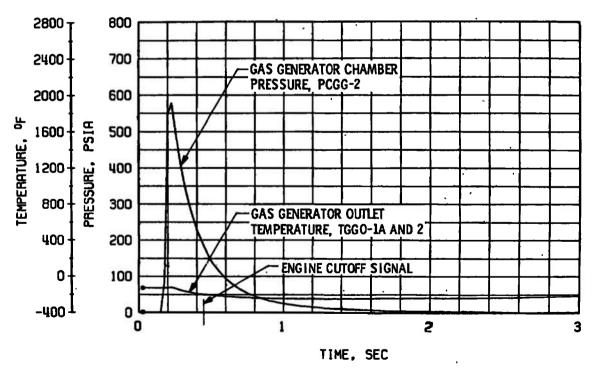
a. Thrust Chamber Fuel System, Start and Shutdown



b. Thrust Chamber Oxidizer System, Start and Shutdown
Fig. 42 Engine Transient Operation, Firing 05A



c. Gas Generator Injector Pressures, Start and Shutdown



d. Gas Generator Chamber Pressure and Temperature, Start and Shutdown
Fig. 42 Concluded

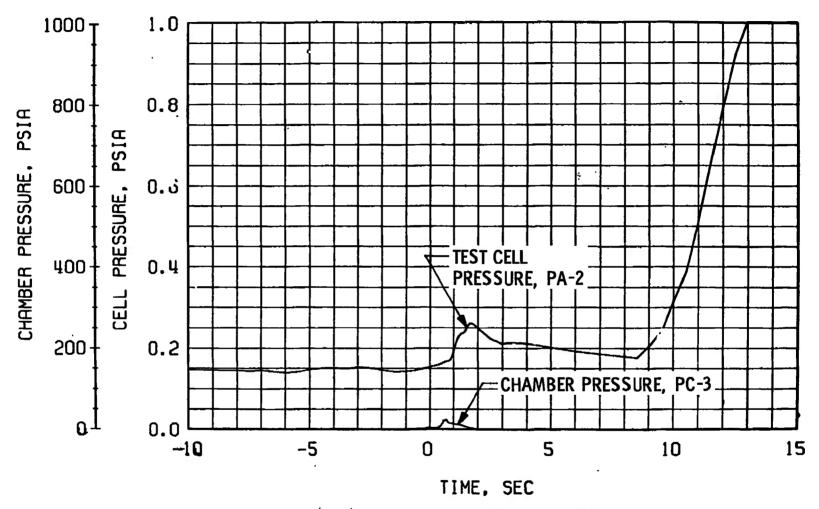
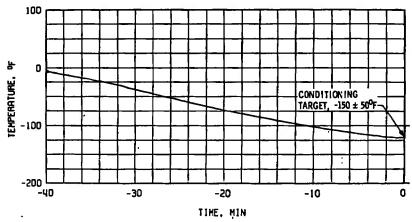
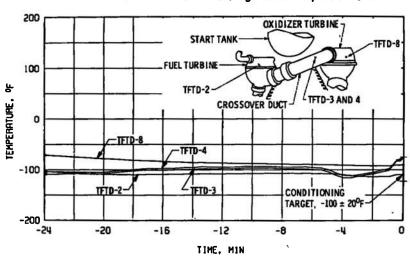
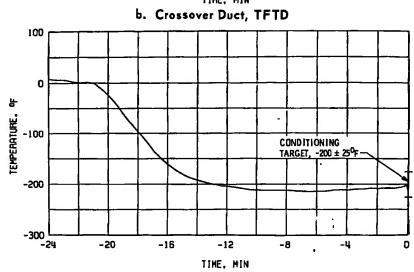


Fig. 43 Engine Ambient and Combustion Chamber Pressure, Firing 05A



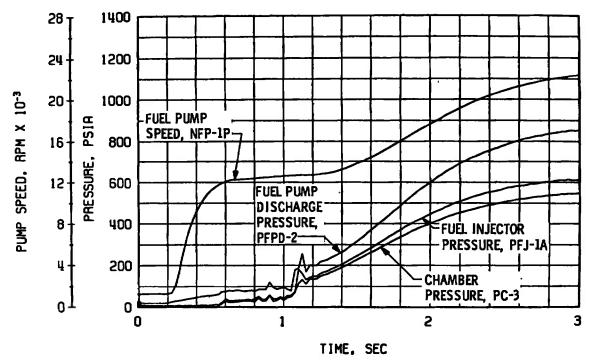
a. Main Oxidizer Valve Second-Stage Actuator, TSOVC-1





c. Thrust Chamber Throat, TTC-1P

Fig. 44 Thermal Conditioning History of Engine Components, Firing 06A



a. Thrust Chamber Fuel System, Start

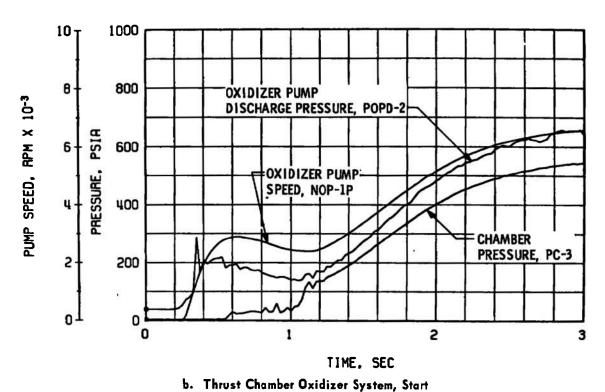
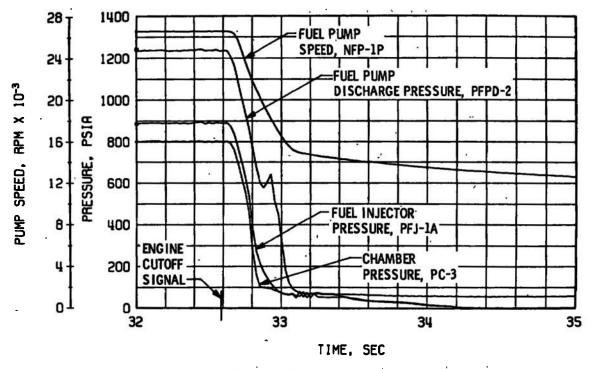
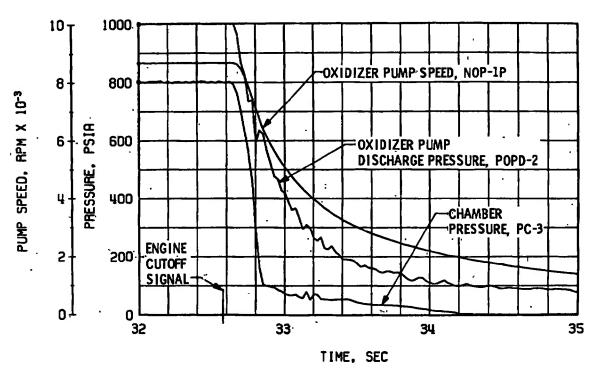


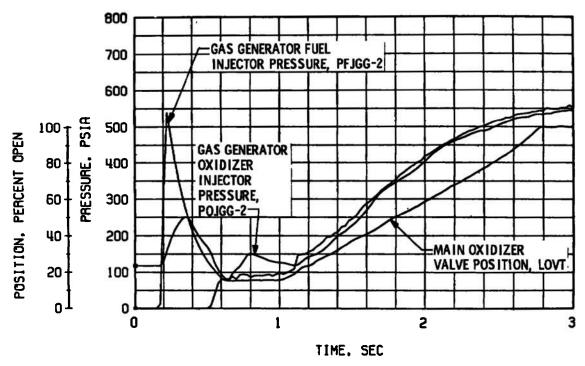
Fig. 45 Engine Transient Operation, Firing 06A



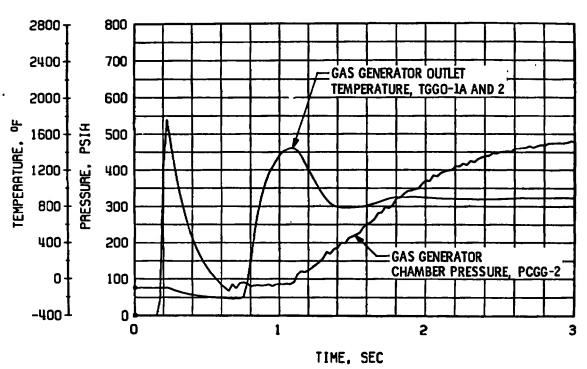
c. Thrust Chamber Fuel System, Shutdown



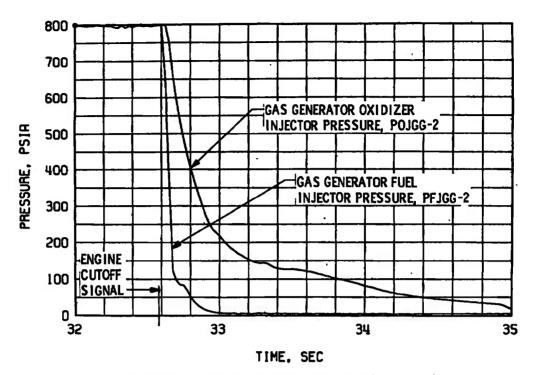
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 45 Continued



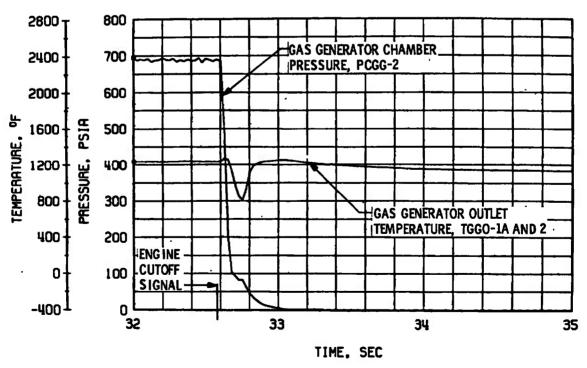
e. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start Fig. 45 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown Fig. 45 Concluded

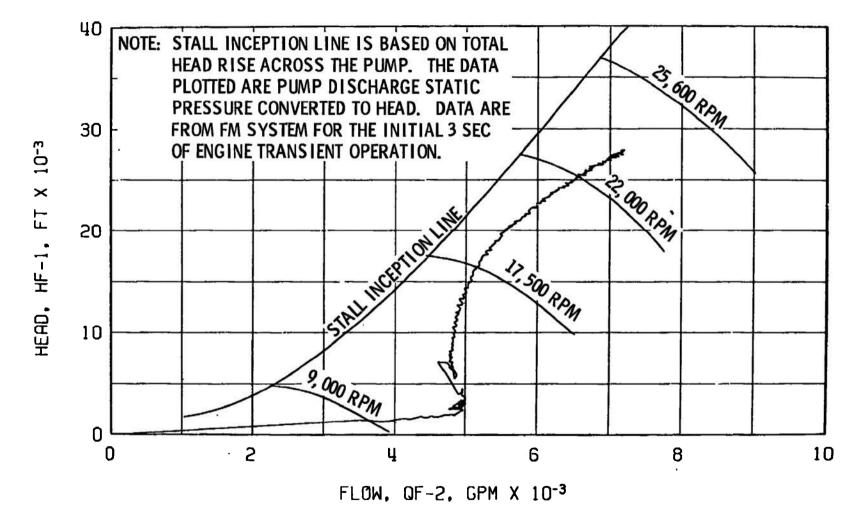


Fig. 46 Fuel Pump Start Transient Performance, Firing 06A

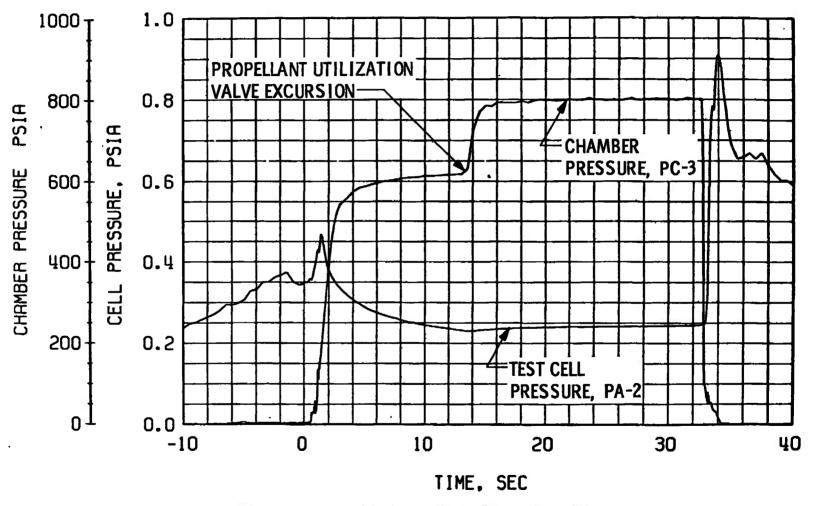
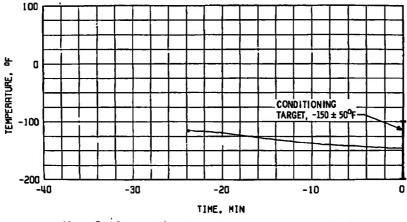
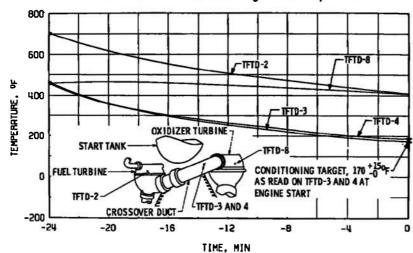


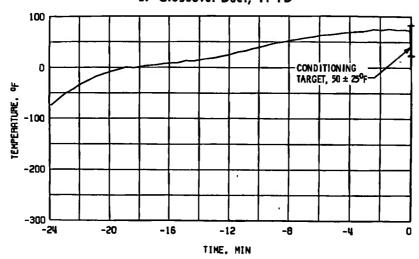
Fig. 47 Engine Ambient and Combustion Chamber Pressure, Firing 06A



a. Main Oxidizer Valve Second-Stage Actuator, TSOVC-1

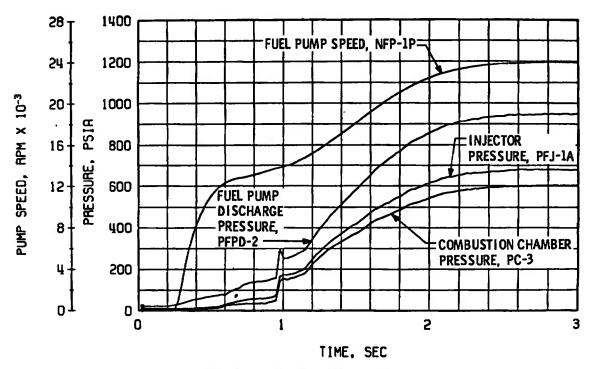


b. Crossover Duct, TFTD



c. Thrust Chamber Throat, TTC-1P

Fig. 48 Thermal Conditioning History of Engine Components, Firing 06B



a. Thrust Chamber Fuel System, Start

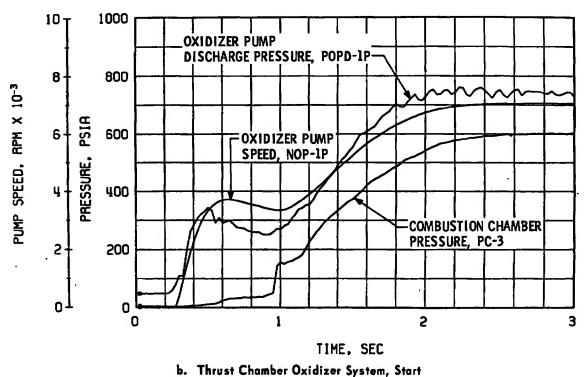
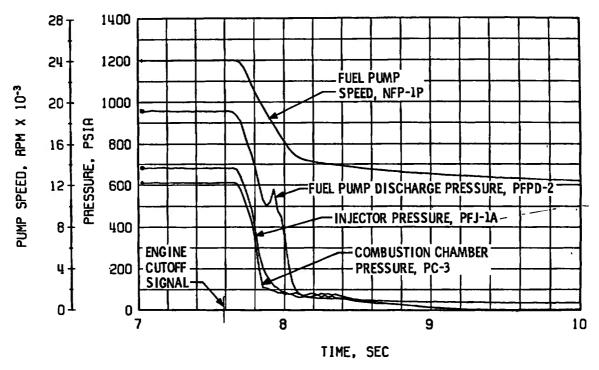
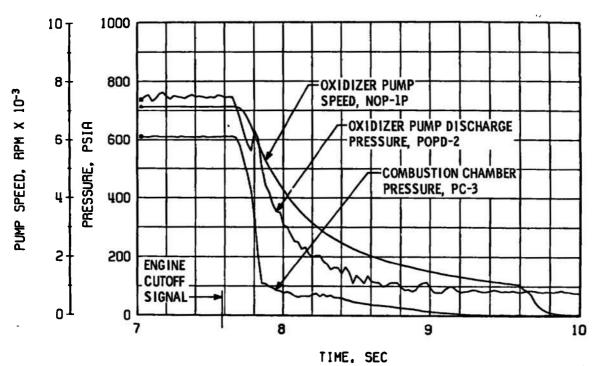


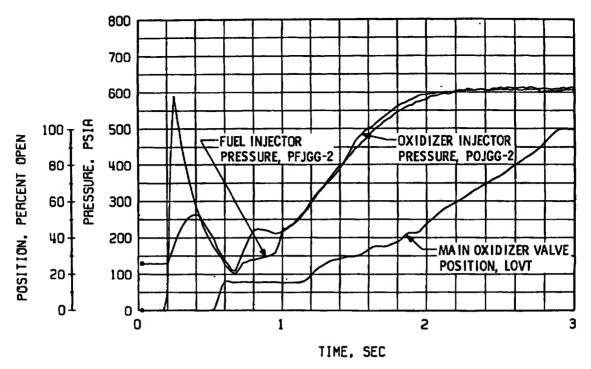
Fig. 49 Engine Transient Operation, Firing 06B



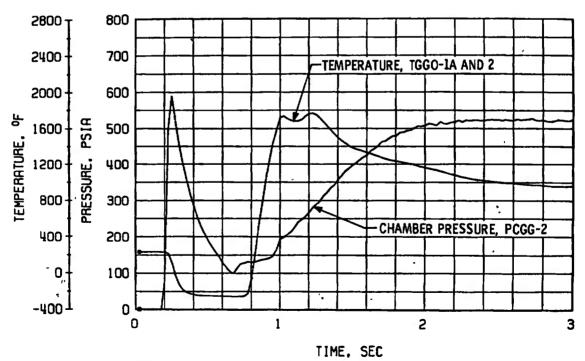
c. Thrust Chamber Fuel System, Shutdown



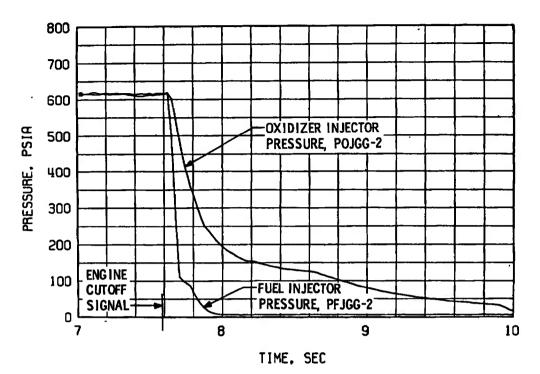
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 49 Continued



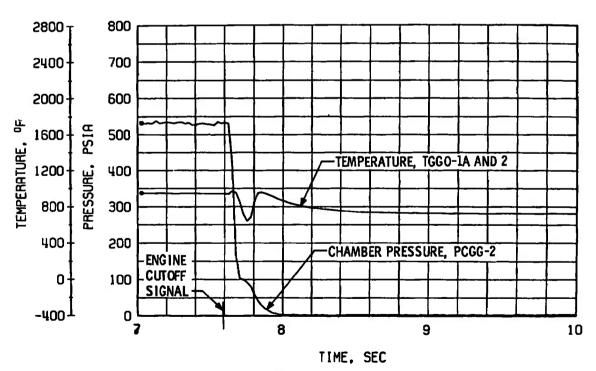
e. Gas Generator Injector Pressures and Main Oxidizer-Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start
Fig. 49 Continued



g. Gas Generator Injector Pressure, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown
Fig. 49 Concluded

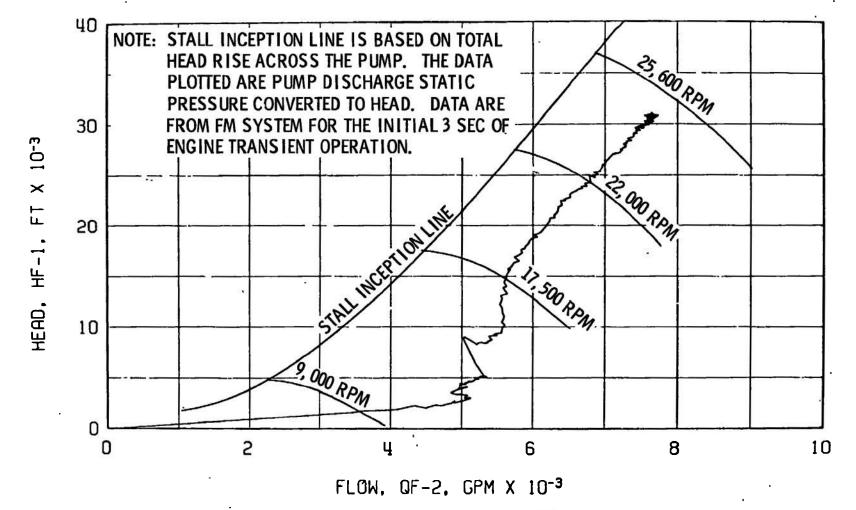


Fig. 50 Fuel Pump Start Transient Performance, Firing 06B

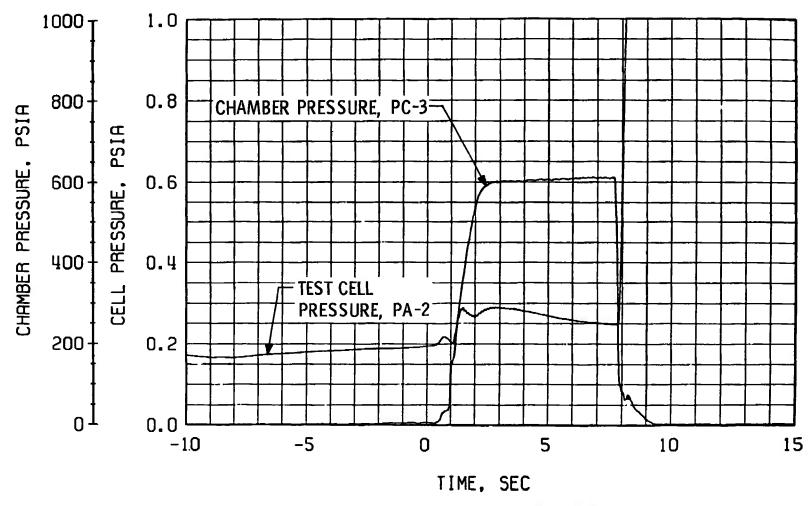


Fig. 51 Engine Ambient and Combustion Chamber Pressure, Firing 06B

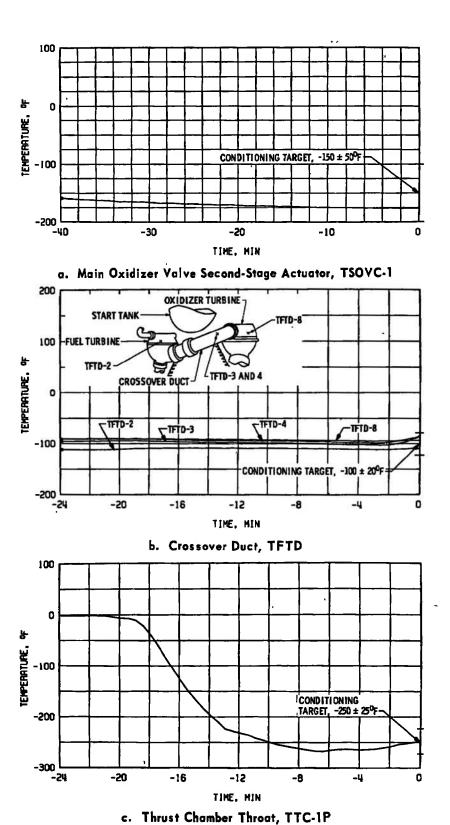
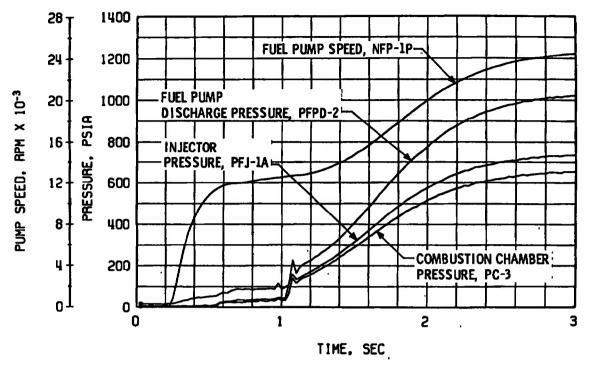
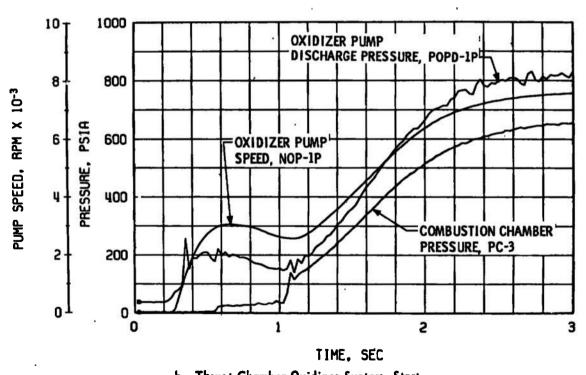


Fig. 52 Thermal Conditioning History of Engine Components, Firing 06C



J. Thrust Chamber Fuel System, Start



b. Thrust Chamber Oxidizer System, Start Fig. 53 Engine Transient Operation, Firing 06C

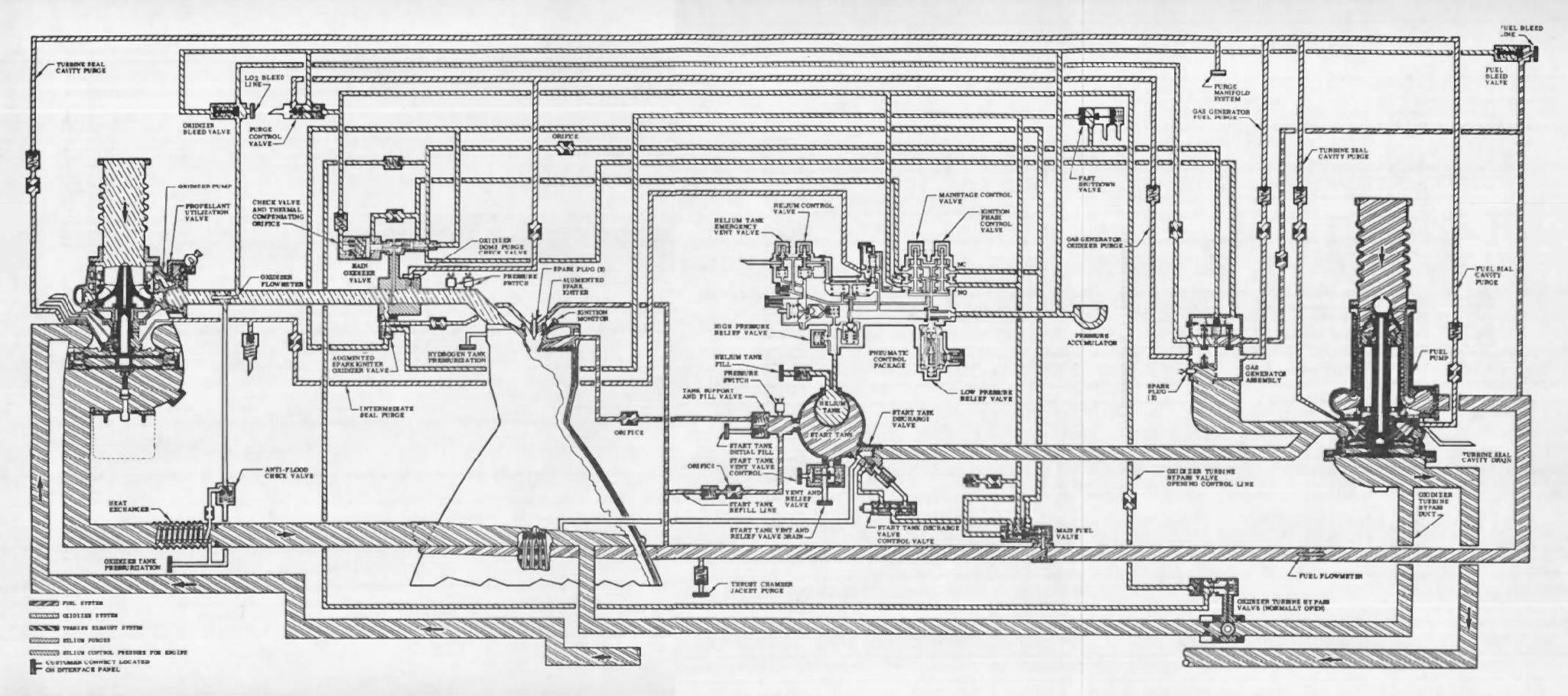
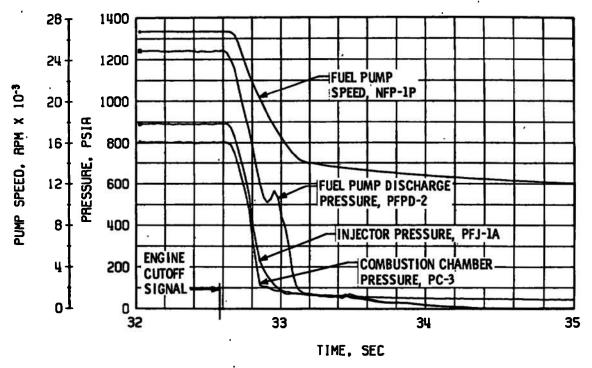
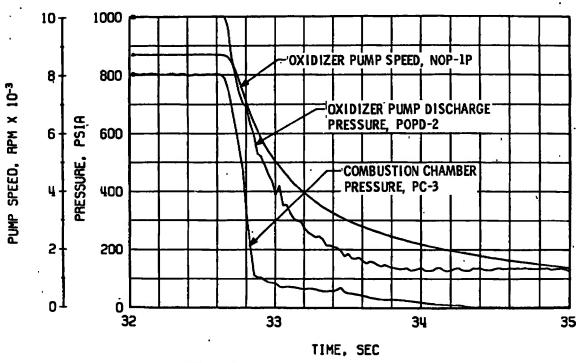


Fig. 5 Engine Schematic

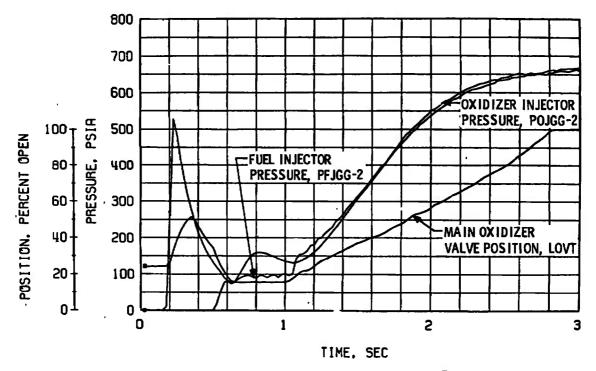
Fig. 6 Engine Start Logic Schematic



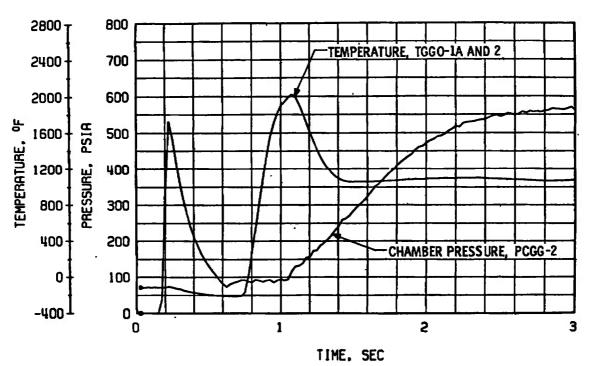
c. Thrust Chamber Fuel System, Shutdown



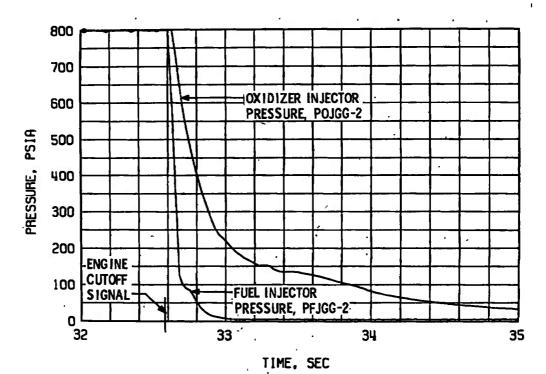
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 53 Continued



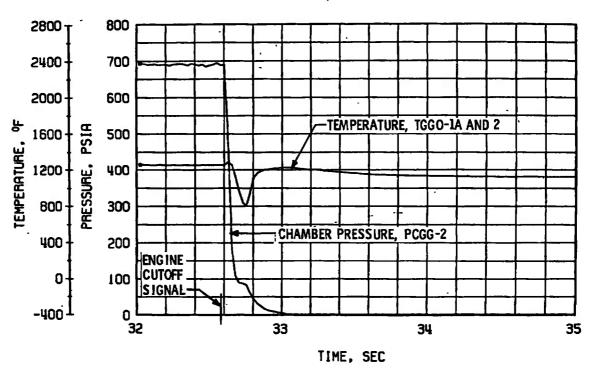
e. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start
Fig. 53 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown Fig. 53 Concluded

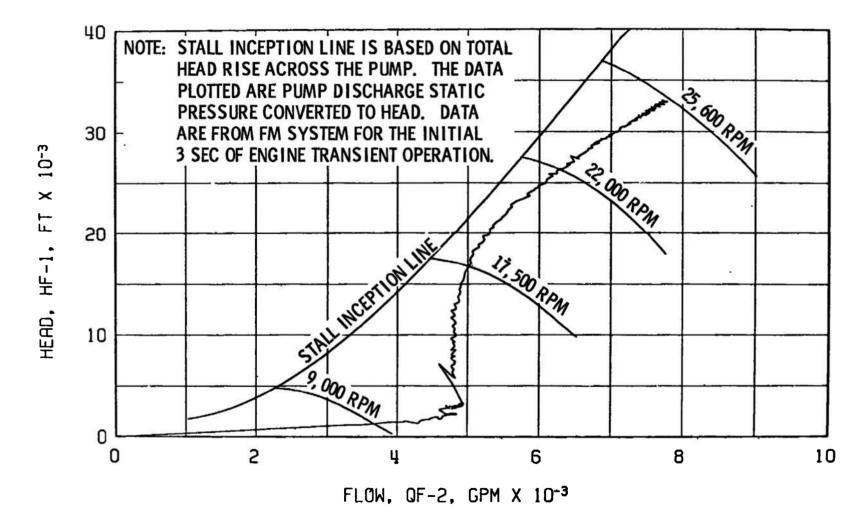


Fig. 54 Fuel Pump Start Transient Performance, Firing O6C

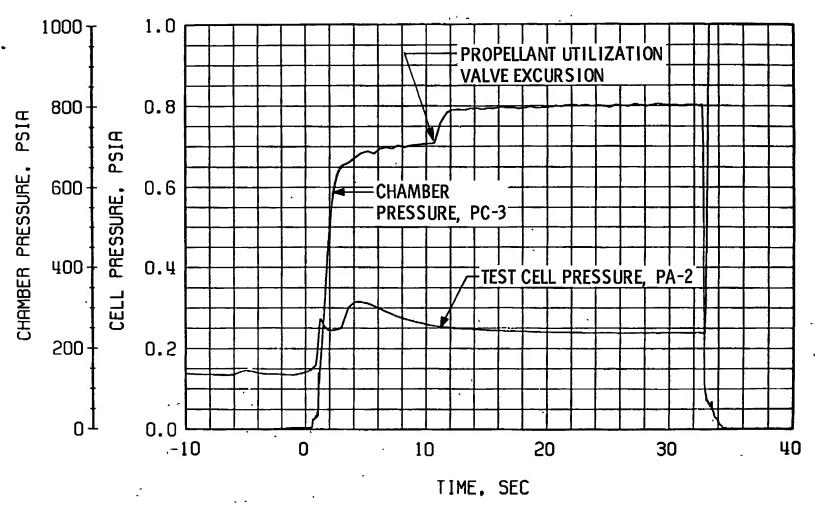
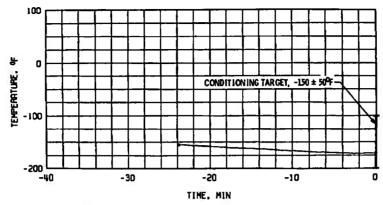
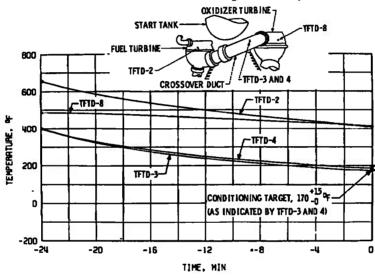
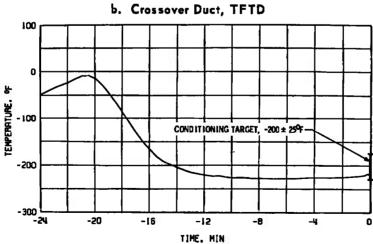


Fig. 55 Engine Ambient and Combustion Chamber Pressure, Firing 06C



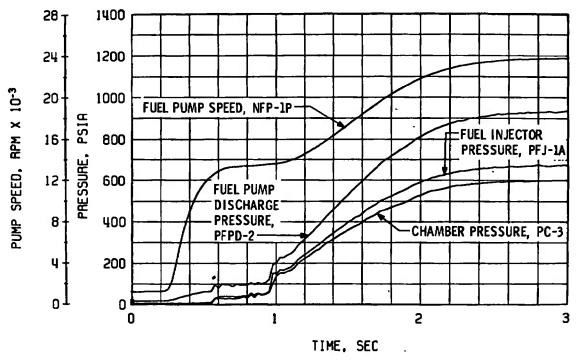
a. Main Oxidizer Valve Second-Stage Actuator, TSOVC-1



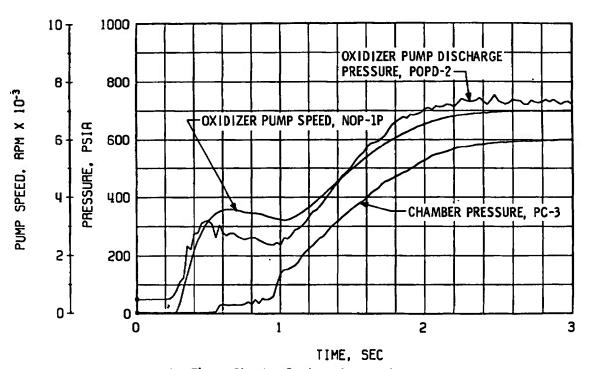


c. Thrust Chamber Throat, TTC-1P

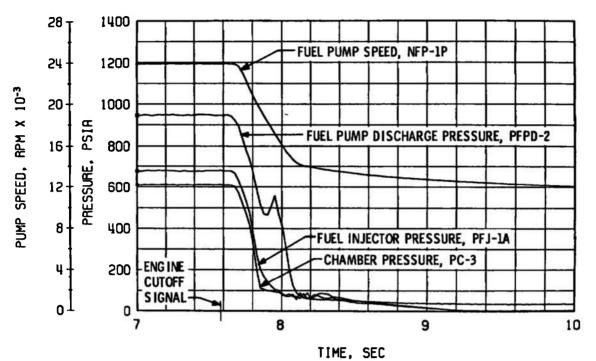
Fig. 56 Thermal Conditioning History of Engine Components, Firing 06D



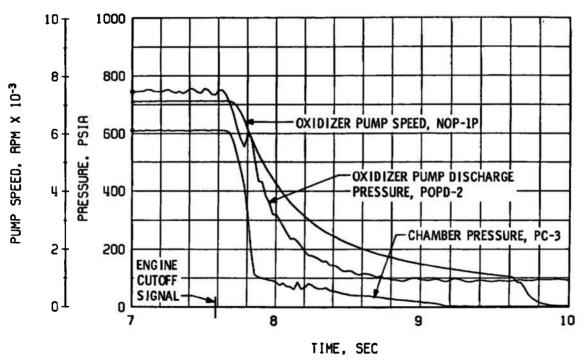
a. Thrust Chamber Fuel System, Start



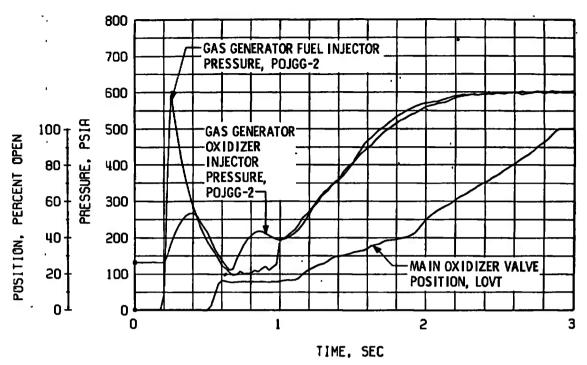
b. Thrust Chamber Oxidizer System, StartFig. 57 Engine Transient Operation, Firing 06D



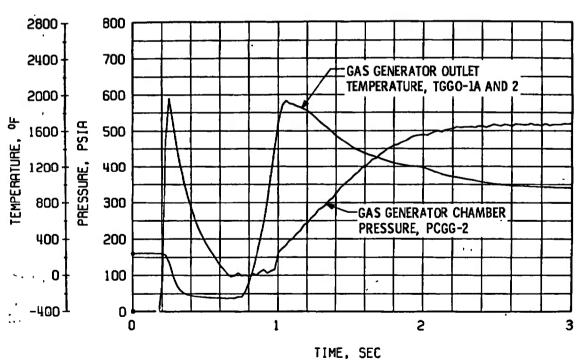
c. Thrust Chamber Fuel System, Shutdown



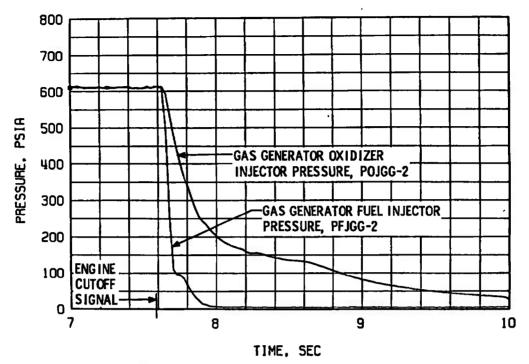
d. Thrust Chamber Oxidizer System, Shutdown
Fig. 57 Continued



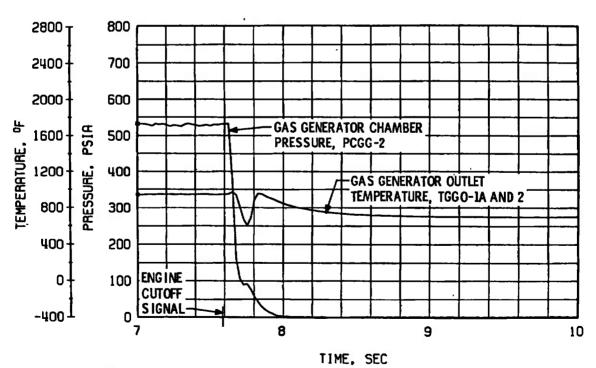
e. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start



f. Gas Generator Chamber Pressure and Temperature, Start Fig. 57 Continued



g. Gas Generator Injector Pressures, Shutdown



h. Gas Generator Chamber Pressure and Temperature, Shutdown
Fig. 57 Concluded



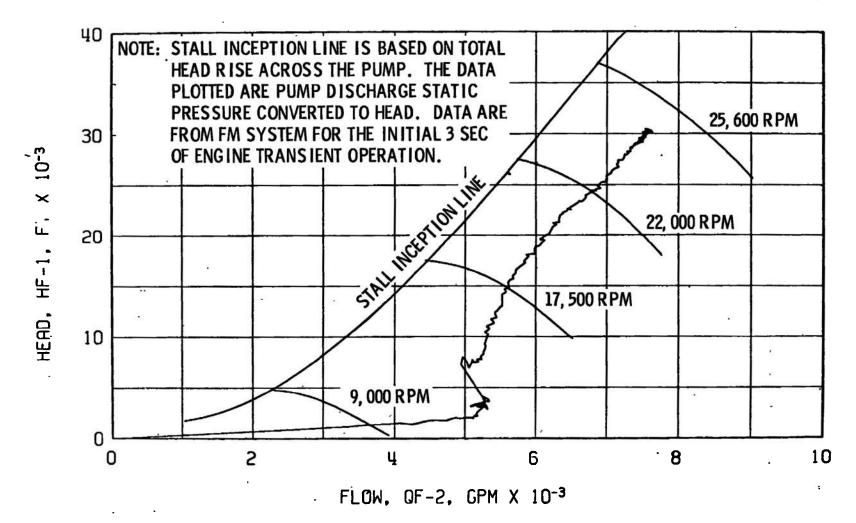


Fig. 58 Fuel Pump Start Transient Performance, Firing 06D

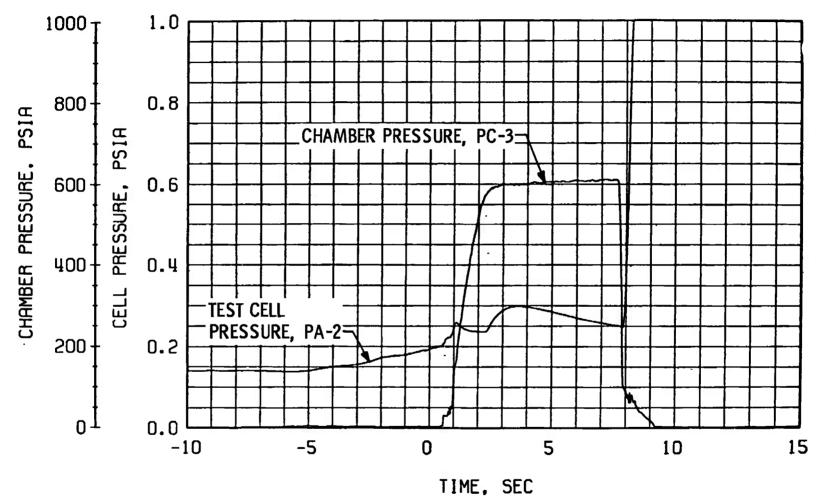


Fig. 59 Engine Ambient and Combustion Chamber Pressure, Firing 06D

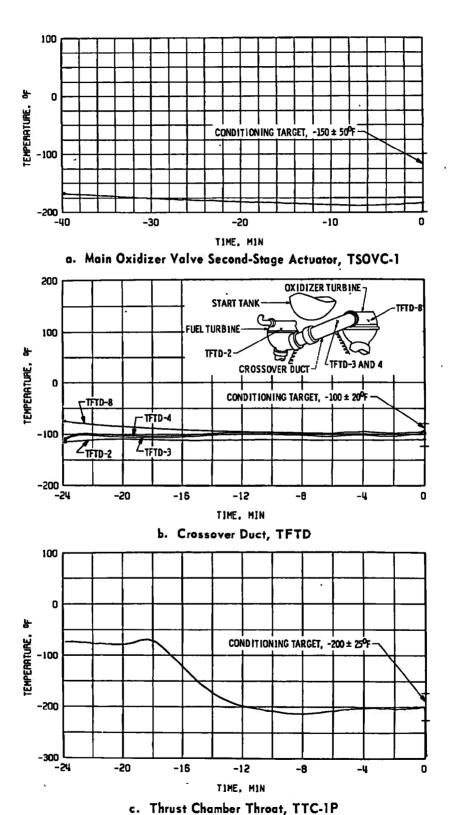
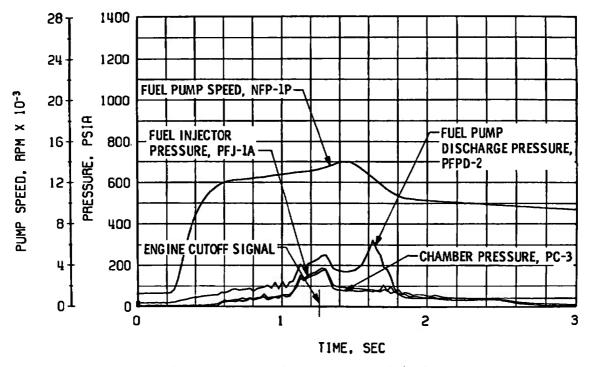
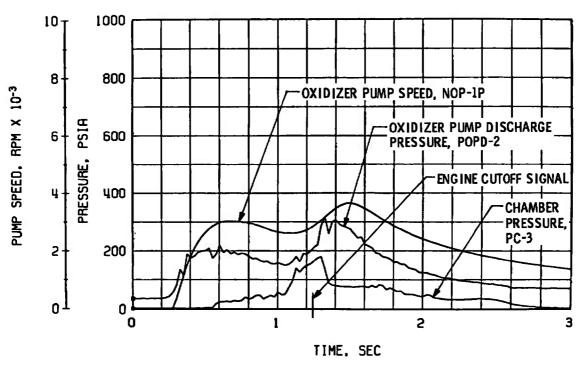


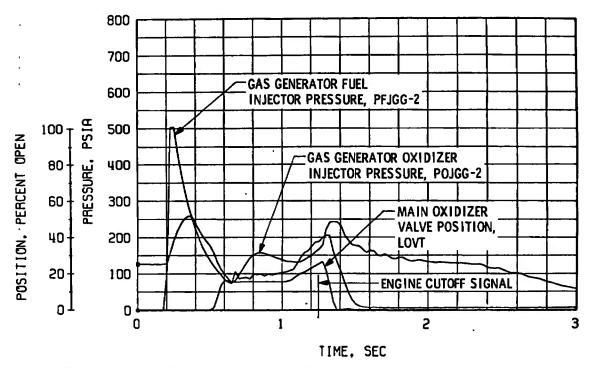
Fig. 60 Thermal Conditioning History of Engine Components, Firing 06E



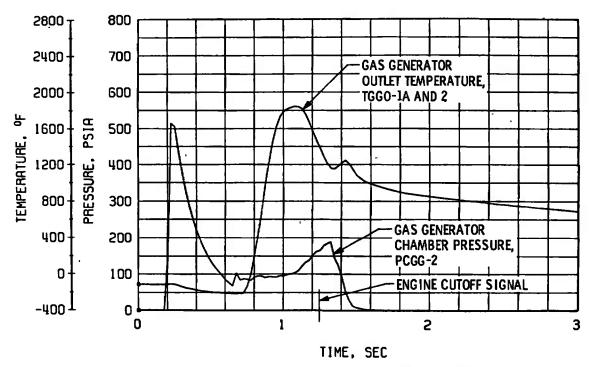
a. Thrust Chamber Fuel System, Start and Shutdown



Thrust Chamber Oxidizer System, Start and Shutdown
 Fig. 61 Engine Transient Operation, Firing 06E



c. Gas Generator Injector Pressures and Main Oxidizer Valve Position, Start and Shutdown



d. Gas Generator Chamber Pressure and Temperature, Start and Shutdown Fig. 61 Concluded

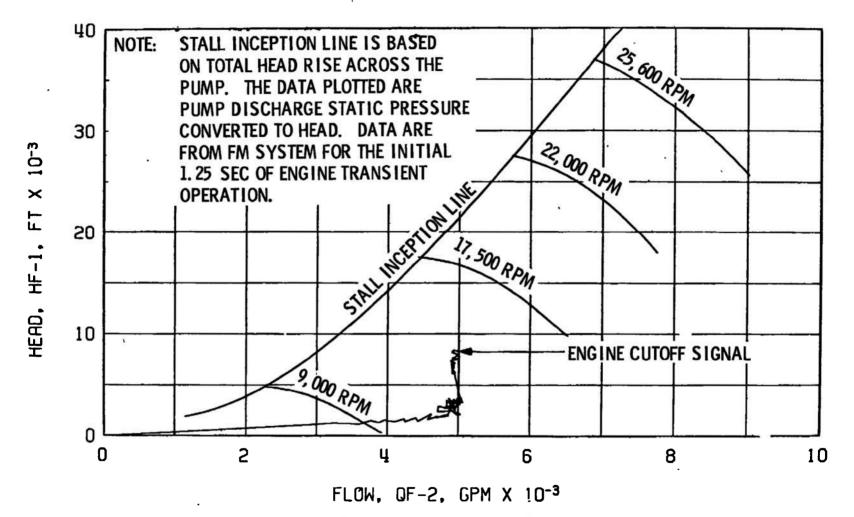


Fig. 62 Fuel Pump Start Transient Performance, Firing 06E

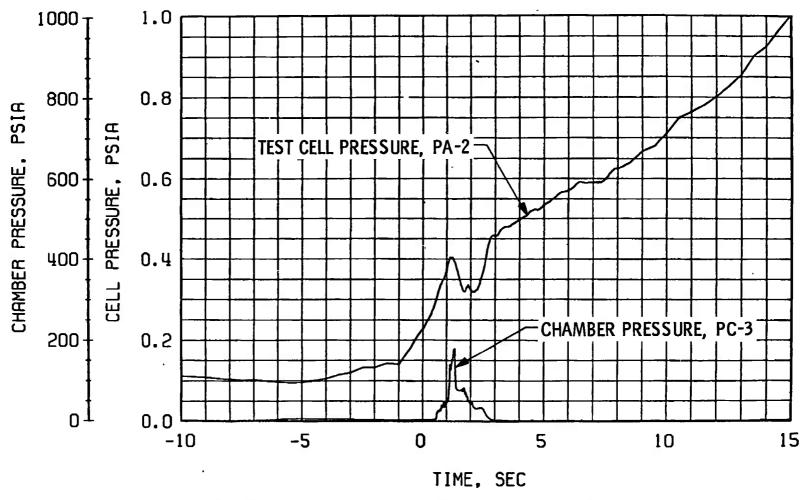


Fig. 63 Engine Ambient and Combustion Chamber Pressure, Firing 06E

TABLE I MAJOR ENGINE COMPONENTS

Part Name	P/N	S/N
Augmented Spark Igniter (Tests 03 and 04)	206280-161	4084016
Augmented Spark Igniter (Tests 05 and 06)	309360-91	4071414
Augmented Spark Igniter Oxidizer Valve	308880	4079065
Auxiliary Flight Instrumentation Package	704090-21	4075163
Electrical Control Package	502670-51	4081742
Fuel Bleed Valve	309034	4084042
Fuel Flowmeter	251225	4074110
Fuel Injector Temperature Transducer	NA5-27441	AA13283F66
Fuel Turbopump Assembly	460390-181	4073647
Gas Generator Control Valve	309040-31	4055754
Gas Generator Fuel Injector and Combustor	308360-11	4090408
Gas Generator Oxidizer Injector and Poppet Assembly	303323	4092975
Helium Control Valve (Three-Way)	WA5-27273	372452
Helium Regulator Assembly	558130-11	4061139
Helium Tank Vent Valve	NA5-27273	379313
Ignition Phase Control Valve (Four-Way)	558069	8313398
Main Fuel Valve	409920	4074288
Main Oxidizer Valve	411031-21	4072666
Main-Stage Control Valve (Four-Way)	558069	8284312
Oxidizer Bleed Valve	309029	4078081
Oxidizer Flowmeter	251216	4075154
Oxidizer Turbine Bypass Valve	409940	4073096
Oxidizer Turbopump Assembly	458175-111	6610105
Pressure-Actuated Purge Control Valve	558126	4073862
Pressure-Actuated Shutdown Valve Assembly	558127-11	4074549
Primary Flight Instrumentation Package	704095-21	4074730
Propeilant Utilization Valve	251351-51	4075182
Restartable Ignition Detect Probe	500750	2125567
Start Tank	307579	0098
Start Tank Discharge Valve	304386	4086957
Start Tank Fill/Relief Valve	557998	4091617
Start Tank Vent and Relief Valve	557848	40 805 17
Thrust Chamber Body	15-205875	4062445
Thrust Chamber Injector Assembly	208021-11	4089721

AEDC-TR-68-238

TABLE II
SUMMARY OF ENGINE ORIFICES

Orifice Name	Part Number	Diameter, Inches Unless Otherwise Noted	Date Effective	Comments
Gas Generator Fuel Supply Fine	RD251-4107	0.488	July 15, 1968	
Gas Generator Oxidizer Supply Line .	RD251-4106	. 0. 284	July 15, 1968	
Oxidizer Turbine Bypass- Valve Nozzle	RD273-8002	1.520	July 15, 1968	
Main Oxidizer Closing Control Line	710437-083 411039X4	8.30 scfm 8.75 scfm	July 5, 1968 August 5, 1968	Thermostatic Orifice
Oxidizer Turbine Exhaust Manifold	RD251-9004	10.00	(1)	
Augmented Spark Igniter Oxidizer Supply Line	309358	0. 125	June 9, 1968	·
Augmented Spark Igniter/Fuel Supply Line		0. 266 0. 302	July 26, 1968 August 5, 1968	No Orifice Used for Test 03

(1)As delivered to AEDC

TABLE III ENGINE MODIFICATIONS (BETWEEN TESTS J4-1901-03 AND J4-1901-06)

Modification Number	Completion Date	Description of Modification
	Test J	1-1901-04
RFD ¹ -AEDC 37-1-68	August 5, 1968	Rerouting of Start Tank Discharge Valve Drain Line
RFD-AEDC 19-68	August 5, 1968	Retiming Main Oxidizer Valve to 1650 +10 msec
RFD-AEDC 42-68	August 5, 1968	Retiming Gas Generator Oxidizer Valve Opening Delay to 150 ⁺⁵ ₋₀ msec
	Test J	4-1901-05

 $^{^{1}\}mathrm{RFD}$ - Rocketdyne Field Directive

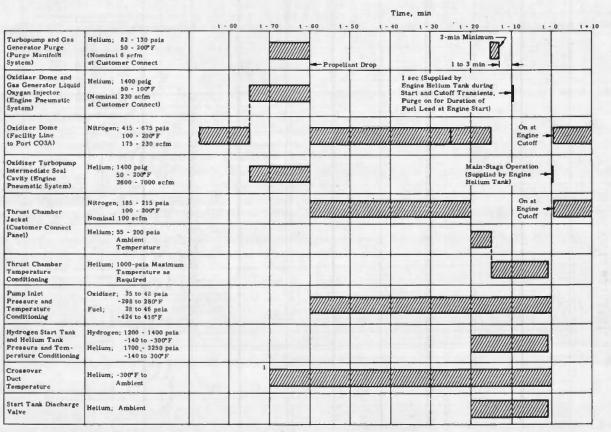
TABLE IV ENGINE COMPONENT REPLACEMENTS (BETWEEN TESTS J4-1901-03 AND J4-1901-06)

Replacement	Completion Date	Component Replaced
	Test J4	-1901-04
UCR ¹ R005151	August 5, 1968	Augmented Spark Igniter Assemblý
	Test J4	- 1901 - 05

¹UCR - Unsatisfactory Condition Report

AEDC-TR-68-238

TABLE V
ENGINE PURGE AND COMPONENT CONDITIONING SEQUENCE



¹Conditioning Temperaturs to be Maintained for the Last 30 min of Pre-Fire

124

TABLE VI SUMMARY OF TEST REQUIREMENTS AND RESULTS

Piete Number 14 1001 00				A		В		C		D
Firing Number: J4-1901-03			Target	Actual	Target	Actual	Target	Actual	Target	Actual
Tima of Day, hr/Firing Data			1343	7/23/68	1408	7/23/68	1637	7/23/69	1704	7/23/
Pressure Attitude at Engine S	itart, ft	(Ref. 1)	100,000	100, 000	100,000	108,000	100,000	106,000	100,000	104,000
Firing Duration, aec®			32.5	32, 575	7.5	7.588	32.5	32.576	7.5	1.264
Fuel Pump Inlet Conditions	Prasa	ure, pala	41.0 +1	41.6	26.5 +1	27.1	26.5 +1	27,1	28,5 +1	27,0
at Engina Start	Temp	eratura, *F	-421.4 ± 0.4	-421.0	-421.4 ± 0.4	-421.3	-421.4 ± 0.4	-421.7	-421.4 ± 0.4	-421.2
Oxidizer Pump Inlet	Prese	ure, psia	33,0 +1	33, 6	45.0 +1	45.1	45.0 +1	45.8	45.0 +1	45.0
Conditions at Engine Start	Temp	erature, *F	-295, 0 ± 0, 4	-295,0	-295,0 ± 0,4	- 295, 3	-295.0 ± 0.4	-295.1	-295.0 ± 0.4	-295, 1
Start Tank Conditions at	Preaa	ure, peis	1400 ± 10	1389	1300 ± 10	1301	1400 ± 10	1369	1300 ± 10	1297
Engine Start	Temp	erature, °F	-200 ± 10	-200	-215 ± 10	-214	-200 ± 10	- 203	-265 ± 10	-268
Helium Tank Conditions	Preea	ure, paim		2068		2240		2065		2023
at Engine Start	Tempe	eratura, °F		-193		-213		-196		- 265
Thrust Chamber Temperature		roat	-90 +20 -10	-64	+50 ± 50	+72	-250 ± 25	-242	+50 ± 50	+62
Conditions at Engine Start/to.	°F Av	verage Engine art/to		-62		-277		-256		+45
		TFTD-2		+34		+455		+33		+436
Crosaover Duct Temperatura at Engina Start, *F®		TFTD4	50 +0	+49	170 +15	+186	50 +0 -50	+50	170 +15	+161
		TFTD-6		+40		+436		+39		+434
Main Oxidizer Valve Second-S Temperature at Engine Start,	Oxidizer Valve Second-Stage Actuator perature at Engine Start, *F®		-150 ± 50	-146	-150 ± 50	-148	-150 ± 50	-159	-150 ± 50	-154
Fuel Lead Time, aec®		- T	3,0	3,018	8.0	7.921	3.0	3.021	8.0	7,937
Propellant in Engine Time, m			30	129		25	30	149	• • • •	27
Propellant Recirculation Tim-	e, min		10	12,5	10	10	10	15	10	16
Start Sequence Logic			Normal	Normal	Normal	Normal	Normal	Normal	Normal	Normal
		TOBS-2A		+54		+16		+37		+4
Gas Generator Oxidizer Suppl Tamperature at Engine Start,		TOBS-3		+ 29		+18		+29		+19
		TOBS-4		+54		+48		+53		+51
Start Tank Discharge Valve B at Engine Start, °F	ody Ten	perature		+31		=4		- 29		-41
Vibration Safety Counta Durat and Occurrence Time, sec, for		ec,		0.976		8 0.960		35 0.964		3 0.9
Gas Ganarator Outlet		Initial Peak		1560		1750		1640		2190
Temperature, °F		Second Peak				1930		N N		
Thrust Chamber Ignition (Pc acc (Ref. to) [©]	100 ps	ia) Time,		0.979		0,961		1. 073		0,939
Main Oxidizer Valva Second-S Movement, sec (Ref. to)©	tage Ini	tial		1.095	1	1.163		1. 095		1.186
Main-Stage Preseure No. 2, a	ac (Ref.	t ₀)0		1.579		1.645		1,604		
Time Chamber Pressure Atta (Raf. to)®	ina 550	pela, eec		1,848		1,993		1.951		
Propellant Utilization Valve F Engine Start/to + 10 acc	osltion,		Null	Null	Open	Open	Null	Null	Open	Open

Notaa:

Data reducad from oaciliogram.

Component conditioning to be maintained within limits for last 15 min before engine atart.

Component conditioning to be maintained within limits for last 30 min before engine start or coast duration, whichaver is longer.

AEDC-TR-68-238

TABLE VI (Continued)

Wilder M			04.A	04	В	04	IC .	0	4D	05	A
Firing Number: J4-1901-		Tergel	Actual	Terget	Actual	Terget	Actual	Target	Actual	Terget	Actuel
Time of Dey, hr/Firing Date		1245	7/31/66	1312	7/31/66	1500	7/31/68	1527	7/31/68	1533	9/8
Preceure Altitude et Engine Ste	ert, ft (Ref. 1)	100,000	78,000	100,000	100,000	100,000	100,000	100,000	100,000	100,000	104,000
Firing Duretion, eac		32.5	25, 020	7.5	7.586	32. 5	32.573	7.5	1.994	32.5	0.446
Fuel Pump Inlet Conditions	Praaaure, psis	26,5 +1	27. 9	28.5 +1	27.0	41.0 ± 1	40,8	41.0 ± 1	40.8	41.0 ± 1	41.3
et Engine Stert	Temperetura,		-421.5	-421.4 ± 0.4	-421.1	-421.4 ± 0.4	-421, 5	-421.4 ± 0.4	-421.3	-420, 4 ± 0, 4	-420.8
Oxidicer Pump inlet	Preceure, pais	45.0 +1	45, 2	45, 0 +1	45,4	45.0 +1	45, 8	45.0 +1	45.8	33,0 ± 1	32.7
Conditiona at Engine Stert	Temperature, '	F -295.0 ± 0.	-295, 1	-295.0 ± 0.4	-295,2	-295, 0 ± 0, 4	-295.1	-295.0 ± 0.4	-294.6	-294,5 ± 0,4	-294, 6
Start Tank Conditions et	Preceure, psia	1400 ± 10	1381	1300 ± 10	1291	1400 ± 10	1400	1300 ± 10	1294	1400 ± 10	1374
Engine Start	Tempereture, '	F -200 ± 10	-216	-265 ± 10	- 266	-200 ± 10	-207	-265 ± 10	- 262	-140 ± 10	-142
Heilum Tank Conditions	Pressura, psis		2041		2160		2158		2207		2122
el Engine Stert	Temperature, *		-204		- 262		-204		- 259		-140
Thrusi Chambar Temperature	Throat	-80 ⁺²⁰	-87	+50 ± 25	+71	-80 +20 -10	-71	+50 ± 25	+76	-160 ⁺²⁰ -10	-154
Conditions at Engine Start/to, *	Y Average En	ine	-71		+33		-79		+36		-142
The Contract of the Contract o	TFTD-2		+35		+424		+16		+433		-101
Croecover Duct Temperature et Engine Start, 'F®	TFTD-	/-4 +50 +0	+45	+170 +10	+185	+50 +0	+34	+170 +10	+167	-100 ± 20	-66
	TFTD-8		+44		+4 t 2		+22		+419		-87
ain Oxidicer Valve Second-Stage Actuator		-150 ± 50	-106	-150 ± 60	-132	-150 ± 50	-151	-150 ± 60	-146	-100 ± 50	-142
Fuel Leed Time, asc		3.0	3,019	6.0	7.934	3.0	3.021	8.0	7,936	1.0	0,999
Propellant in Engine Time, mir	1	30				30				3.0	
Propellant Recirculation Time,	min	10	10	10	17.5	10	24.5	10	10	10	10
Stert Sequence Logic		Normal	Normal	Normal	Normal	Normal	Normel	Normel	Normal	Normel	Normel
	TOBS-2	A	+60		+29		+41	1	+10		+24
Gas Generetor Oxidieer Supply Temperature et Engine Stert, "!			+44		+31		+37		+27		+36
	TOBS-4		+59		+49		+52		+37		+58
Start Tank Discharge Valve Bod et Engine Stert, "F	ly Temperature		+55		+3		-61		-53	50 ± 25	+61
Vibrelioo Sefsty Counte Duralio end Occurrence Time, acc, fro			0,978		15 1.049		0.958		9 0.948		
Gea Generelor Outlet	Initial F	eek	1670		1940		1960		2010		
Temperature, 'F	Second	onle	1750		2120		7	8	2160		
Thrus! Chamber Ignition (Pc = :	100 psia) Time,		0.962		0,945		0.958		0.948		•••
ain Oxidiser Valve Second-Stage Initial overment, eec (Ref. to)©			1.085		1.198		1, 111		1,222		
Mein-Stage Preceure No. 2, acc	(Ref. to)		1,582		1,637		1.579		1.642		
Time Chamber Pressure Altain Ref. 10) [©]	s 550 paia, eec		1.821		2.005		1.807	-	1.984		
Propellant Utilization Velve Pos Engine Start/to + 10 eec	sitlon,	Null	Null	Open	Open	Null	Null Closed	Open	Open	Null	Null

Note:

Dele reduced from oscillogram.

Component conditioning to be mainteined within limite for last 15 min before engine elert.

Component conditioning to be maintained within limits for lest 30 min before engine elert or coeet duration, whichever is longer.

TABLE VI (Concluded)

Firing Number: J4-1901-06				A		В		С		D		E
			Target	Actual	Target	Actual	Target	Actual	Target	Actual	Target	Actual
Time of Day, hr/Firing Data			1446	6/15/86	1514	6/15/66	1846	8/15/68	1917	8/15/66	2027	8/15/6
Pressure Altitude at Engine 5ts	art, ft	(Ref. 1)	100,000	69,000	100,000	66,000	100,000	103,000	100,000	103,000	100,000	110,000
Firing Duration, secO			32.5	32,574	7.5	7.569	32.5	32,574	7.5	7,585	1.25	1,251
Pull Pump Intel Conditions		ure, psis	26.5 +1	27. 2	26.5 +1	26, 8	28.5 +1	26. 2	26.5 +1	26, 4	26,5 +1	27. 2
		ersturs, *F	-421,4 ± 0,4	-421, 3	-421.4 ± 0.4	-420.6	-421.4 ± 0.4	-421.7	-421. 4 ± 0.4	-421, 2	-421.4 ± 0.4	-421.2
Oxidizat Lamb litter	Presa	ure, psia	33.0 ± 1	33.7	45.0 +1	45,4	33.0 +1	33, 7	45,0 +1	45, 2	33, 0 +1	32, 0
		ersture, °F	-295,0 ± 0,4	-295.4	-295.0 ± 0,4	-265, 2	-295.0 ± 0.4	-294.9	-295.0 ± 0.4	-294,7	-295.0 ± 0.4	-293.9
Start Lank Conditions at		ure, pals	1250 ± 10	1258	1300 ± 10	1313	1250 + 10	1263	1300 ± 10	1312	1250 ± 10	1254
Engine Start	Temp	ersture, *F	-140 ± 10	- 14 3	-265 ± 10	-267	-140 ± 10	-140	-265 ± 10	-285	-140 ± 10	-137
EVELTATED V SURY COMPATITIONS	Press	ure, psis		2091		2081		2006		2081		2445
at Engine Start	Temp	ersture, °F		-129		-257		-136		-261		-144
Thrust Chamber Temperature		roat	-200 ± 25	-203	+50 ± 25	+72	-250 ± 25	-246	-200 ± 25	-217	-200 ± 25	-169
Conditions at Engine Start/to, *	F Av	erage Engine art/to		-185		+24		-342		-206		-201 -3
		TFTD-2		-109		+409		-110		+409		-110
Crossover Duct Tampersture		TFTD-3/-4	-100 ± 20	-76	±170 +15	+174	-100 ± 20	-88	+170 +15	+173	-100 ± 20	-95
		TFTD-6		-60		+406		-93		+415		-100
Main Oxidizer Valve Second-Sta Temperatura at Engine Start, *	n Oxidizer Valve Second-Stage Actuator		-150 ± 50	-121	-150 ± 50	-147	-150 ± 50	-176	-150 ± 50	-171	-150 ± 50	-184
Fuel Lead Time, sec			8,0	7.936	6.0	7.939	3,0	3,022	6.0	7,936	6,0	7,938
Propellant in Engine Tims, mir		-	30				30				30	
Propellant Recirculation Tima,	min		10	10	10	14	10	10	10	11,5	10	10
Start Sequence Logic	_	-	Normal	Normal	Normal	Normal	Normal	Normal	Normal	Normal	Normal	Normal
C C	1.7-	TOBS-2A		+32		+3		~6		-10		-19
Gas Generator Oxidizer Supply Temperatura at Engine Start, *:		TOBS-3		+30		+19		+19		5		+9
		TOBS-4		+46		+50		+41		+34	8	+42
Start Tank Discharge Valve Bod at Engine Start, °F	dy Tem	nparature		+78		+24		+12		-16		+26
Vibration Safety Counts Duratio and Occurrence Time, sac, from		ec,		75		0, 950		1, 052		25 0. 960		
Gas Generator Outlet		Initial Peak		1450		1730		2020		1930		1640
Temperature, °F		Sacond Peak				1760				- 3		
Thrust Chamber Ignition ($P_c = 3$ sec (Ref. to) \mathbb{O}	100 ps	ia) Time,		1. 091	10,00	0.953		1.062		0,972	1	1.093
Main Oxidizer Valve Second-Sta Movement, sec (Ref. to)®	Oxidizer Valve Second-Stage Initial ement, sec (Ref. to)			0, 967		1.115		1.004		1,098		1. 014
Main-Stage Pressure No. 2, sec	(Ref.	t _O)O		2. 161		1,768		1.804		1.689		
Time Chamber Prassurs Attain. (Ref. to) ©	s 550 j	psia, aec		3, 233		2,013		2. 124		2, 090		
Propellant Utilization Valva Pos Engine Start/to + 10 sec	ition,		Open Closed	Open Closed	Open	Open	Null Closed	Null	Open	Open	Nul1	Null

Notas:
Obta reduced from oscillogram.

Ocomponent conditioning to be maintained within limits for last 16 min before engine start.

Ocomponent conditioning to be maintained within limits for last 30 min before angine start or coast duration, whichavar is longer.

TABLE VII ENGINE VALVE TIMINGS

												Sta	rt											
Firing Number		Start	Tank Dia	scharge V	/alve		Main	Fuel V	alve		Oxidizer irst Stag			Oxidize:	r Valve		General			Gener		Oxidizer Turbine Bypass Valve		
J4-1801-	Time of Opening Signal	Valve Delay Time, eec	Valve Opening Time, sec	Time of Closing Signal	Valve Delay Time,	Valve Closing Time, sec	Time of Opening Signal	Valve Delay Time, sec	Valve Opening Time, sec	Time of Closing Signal	Valve Delay Time, sec	Valve Closing Time, sec												
03A	0.0	0. 128	0. 111	0.450	0.128	0.248	-3.018	0.076	0.102	0.450	0.056	0.052	0.450	0.645	1.882	0.450	0.108	0.030	0.450	0. 185	0.077	0.450	0.211	0. 286
03B	0.0	0. 131	0.113	0.450	0.131	0.251	-7.821	0.073	0.108	0.450	0,058	0.052	0.450	0.733	1.798	0.450	0.112	0.033	0.450	0.191	0.088	0.450	0.208	0. 291
03C	0.0	0, 136	0.118	0, 449	0, 131	0.258	-3.021	0.085	0.088	0.449	0.057	0.051	0.448	0.848	1, 902	0.449	0.112	0,031	0.448	0.167	0.078	0.448	0.209	0.289
03D	0.0	0.137	0. 121	0.450	0.135	0.253	-7.837	0.073	0.114	0, 450	0.056	0.052	0.450	0.736		0.450	0.113	0.030	0.450	0.186	0.091	0.450	0, 201	0. 288
Final Sequence	0.0	0. 086	0.088	0,449	0.126	0.238	-1.000	0,055	0.103	0.449	0.048	0.047	0.449	0.588	1.743	0.448	0.082	0.033	0.449	0, 141	0.071	0.449	0, 182	0. 281
04A	0.0	0. 127	0. 109	0, 450	0.128	0.244	-3.018	0.079	0.103	0.450	0, 058	0, 051	0.450	0.635	1,898	0.450	0.106	0, 031	0.450	0. 183	0.080	0.450	0.218	0, 286
04B	0.0	0.130	0.118	0, 450	0, 132	0.248	-7.834	0.074	0.114	0.450	0.058	0,052	0.450	0.746	1, 765	0.450	0.108	0.031	0, 450	0.188	0.088	0.450	0.206	0.287
04C	0.0	0.137	0.128	0,449	0.134	0.258	-3.021	0.073	0.111	0,449	0.056	0.053	0.449	0.662	1.883	0.449	0.111	0.031	0.448	0. 187	0.084	0.449	0.218	0.286
04D	0.0	0.136	0.123	0, 448	0.135	0.259	-7, 838	0.076	0.113	0.448	0.055	0.053	0.448	0.774		0.448	0.112	0.032	0.448	0.182	0.092	0.448	0. 207	0.280
Final Sequence	0.0	0.086	0.082	0.450	0.127	0.241	-0.877	0.058	0, 106	0.450	0.051	0.044	0.450	0.604	1.737	0,450	0.084	0.032	0.450	0.142	0.068	0.450	0.187	0.288
05A	0.0	0. 123	0.108	0.446	1.718	0.431	-1.001	0.088	0.086															
Final Sequence	0.0	0.090	0. 089	0, 450	0.126	0, 238	-1,000	0.057	0. 101	0.450	0.053	0.048	0.450	0, 475	1,850	0.450	0.078	0.038	0.450	0, 153	0.081	0.450	0.188	0.282
06A	0.0	0.110	0.103	0.450	0.116	0.248	-7,838	0.083	0.088	0,450	0.056	0.051	0.450	0.537	1.761	0.450	0.107	0.038	0.450	0, 188	0.084	0.450	0. 202	0.286
06B	0, 0	0.126	0.114	0.451	0.128	0.242	-7.839	0.081	0.115	0.451	0.057	0.051	0.451	0.664	1, 743	0.451	0.117	0.033	0.451	0. 207	0. 108	0, 451	0. 211	0. 288
08C	0.0	0.123	0.112	0.448	0.125	0.251	-3, 022	0.085	0.116	0.448	0.059	0.055	0.448	0.556	1, 787	0.448	0.118	0. 038	0.448	0.188	0. 101	0.448	0.217	0.298
08D	0.0	0. 132	0.117	0.448	0. 127	0. 251	-7.836	0.084	0.119	0.448	0.058	0.053	0.448	0.648	1, 767	0.448	0.118	0. 038	0.448	0, 212	0. 104	0.448	0.213	0. 283
06E	0,0	0, 133	0.111	0.449	0, 124	0. 251	-7.838	0. 082	0.116	0.449	0.058	0.052	0.448	0.565		0.448	0.116	0.035	0.448	0. 203	0, 108	0.448	0.203	0. 281
Final Sequence	0.0	0, 092	0.083	0.446	0, 126	0, 237	-0.898	0.047	0.092	0.446	0.052	0.047	0.448	0. 480	1, 846	0,448	0.088	0.037	0.448	0.154	0.078	0.448	0. 185	0, 280

Notes: 1. All valve signal times are referenced to t₀.

2. Valve delay time is the time required for initial valve movement after the valve "open" or "closed" colenoid has been energized.

3. Final sequence check is conducted without propellanta and within 12 hr before testing.

4. Data reduced from oscillogram.

TABLE VII (Concluded)

							SI	hutdown							
Firing Number	Main	Fuel V	alve	Main O	xidizer	Valve		Genera uel Pop			s Gener dizer Po			lzer Tu pass Va	
J4-1901-	Time of Closing Signal	Valve Delay Time, sec	Valve Closing Time, sec	Time of Opening Signal	Valve Delay Time, sec	Valve Opening Time, sec									
03A	32.573	0.108	0.302	32,573	0.086	0.183	32,573	0.068	0.013	32.573	0.032	0.013	32.573	0.251	0.518
03B	7,586	0.099	0.290	7.586	0.078	0.176	7. 586	0.075	0.016	7.586	0.036	0.015	7.586	0.234	0.486
03C	32,573	0.111	0.330	32.573	0.088	0.184	32, 573	0.069	0.015	32.573	0.031	0.015	32.573	0.252	0.513
03D	1, 263	0.096	0.295	1.263			1.263	0.081	0.020	1.263	0.041	0.018	1.263	0.158	0.504
Final Sequence	4.704	0.081	0.224	4.704	0.053	0.123	4.704	0.090	0.037	4.704	0.061	0.022	4.704	0.218	0.574
04A	25.020	0.107	0.301	25.020	0.081	0.176	25.020	0.068	0.014	25,020	0.031	0.013	25.020	0.247	0.543
04B	7,586	0.101	0. 294	7.586	0.076	0.174	7.586	0.074	0.015	7.586	0.036	0.015	7.586	0.217	0.492
04C	32, 573	0.108	0. 315	32.573	0.086	0.186	32.573	0.069	0.015	32,573	0.031	0.014	32.573	0.249	0.528
04D	1.994	0.096	0.293	1.994			1.994	0.076	0.016	1.994	0.036	0.014	1.994	0.198	0.499
Final Sequence	6.447	0.081	0.224	6.447	0.062	0. 121	6.447	0.094	0. 037	6.447	0.061	0.024	6.447	0.222	0.588
05A	0.448	0.098	0.271												
Final Sequence	4.634	0.079	0.226	4.634	0.053	0.123	4.634	0.092	0.034	4.634	0.059	0.026	4.634	0.218	0.578
06A	32.573	0.107	0.313	32.573	0.083	0.178	32.573	0.066	0.012	32,573	0.031	0.013	32.573	0.254	0.574
06B	7.588	0.103	0.316	7.588	0.078	0.174	7.588	0.074	0.016	7.588	0.036	0.015	7.588	0.233	0.525
06C	32.571	0. 121	0.365	32.571	0.089	0. 191	32.571	0.074	0.015	32.571	0.033	0.014	32.571	0. 276	0.616
06D	7.584	0.109	0,341	7.584	0.081	0. 179	7.584	0.079	0.016	7.584	0.037	0.015	7.584	0.245	0.522
06E	1.247	0.109	0.347	1. 247			1.247	0.087	0.026	1.247	0.051	0.022	1.247	0.169	0.564
Final Sequence	6.695	0.079	0. 222	6.695	0.064	0.118	6.695	0.093	0.037	6.695	0.059	0.026	6.695	0.218	0.576

Notes: 1. All valve signal times are referenced to t₀.

2. Valve delay time is the time required for initial valve movement after the valve "open" or "closed" solenoid has been energized.

3. Final sequence check is conducted without propellants and within 12 hr before testing.

4. Data reduced from oscillogram.

TABLE VIII
ENGINE PERFORMANCE SUMMARY

Pinin - Manual	14 1001		03A		03C	7	04C		06A		06C
Firing Number	74-1301-	Site	Normalized								
	Thrust, lbf	230, 597	227,639	229, 956	227, 390	229, 450	226, 787	229, 959	227, 274	230, 360	227, 645
	Chamber Pressure, psla	788.9	775.1	786.8	774.4	785.5	772.4	787. 4	773.9	788.6	775.4
Overall Engine	Mixture Ratio	5.498	5 507	5.584	5.574	5.583	5.597	5.606	5.621	5.638	5.819
Performance	Fuel Weight Flow, lbm/sec	84.11	82.57	83. 25	81.87	82.76	81. 27	82.59	81.07	82,54	81.37
	Oxidizer Weight Flow, lbm/sec	462.3	454.7	463.2	456.4	462.0	454.9	463.1	455.7	465.3	457.2
	Total Weight Flow, lbm/sec	546.4	537.3	546.5	538.3	544.8	536, 2	545.6	536.8	547.9	538.6
Thrust	Mixture Ratio	5.701	5.715	5.773	5.787	5. 788	5.806	5. 818	5.837	5.849	5. 832
Chamber	Total Weight Flow, lbm/sec	539.3	530. 2	539.4	531.2	537.8	529.2	538.6	529.8	540.8	531.8
Performance	Characteristic Velocity, ft/sec	8017	8011	7994	7989	8005	7999	8012	8005	7992	7995
	Pump Efficiency, percent	73.8	73.8	73.8	73.8	73.7	73. 7	73.9	73.9	74.0	74.0
	Pump Speed, rpm	26, 829	26,573	26,640	26, 449	26,518	26, 319	26, 529	26,329	26,671	26,478
Fuel Turbopump	Turbine Efficiency, percent	60.8	60.6	60.3	60.2	59.4	59.2	59.4	59.2	59.4	59.3
Performance	Turbine Pressure Ratio	7. 38	7. 38	7. 30	7. 29	7.33	7, 33	7, 34	7.34	7. 33	7.33
	Turbine Inlet Temperature, °F	1230	1210	1230	1214	1273	1256	1242	1225	1261	1239
	Turbine Weight Flow, lbm/sec	7. 11	7. 03	7. 08	7. 01	7. 02	6.94	7. 07	6.98	7. 08	7.00
	Pump Efficiency, percent	80.3	80. 2	80.3	80. 3	80.3	80. 3	80.3	80.3	80.4	80, 3
	Pump Speed, rpm	8707	8633	8724	8650	8695	8620	8673	8602	8702	8624
Oxidizer Turbopump	Turbine Efficiency, percent	48.4	48.2	48.7	48.4	49.2	48. 9	48.9	48,7	49.1	48.9
Performance	Turbine Pressure Ratio	2.58	2, 58	2.60	2.59	2.59	2, 58	2, 59	2.59	2.58	2,58
	Turbine Inlet Temperature, °F	827.4	813.3	831.6	819.7	843.7	832.0	832. 9	821.1	847.5	831.4
	Turbine Welght Flow, lbm/sec	6. 23	6.16	8. 19	6.13	6.14	6.07	6.18	6, 11	6.19	6.13
Gas Generator	Mixture Ratio	0.957	0.946	0.957	0.948	0.983	0.973	0.964	0, 955	0.976	0.963
Performance	Chamber Pressure, psia	691.3	681.4	688.0	679.2	686.6	677.2	688.0	678.3	691.2	681.6

Notes: 1. Site data are calculated from test data.

2. Normalized data are corrected to standard pump inlet and engine ambient pressure conditions.

3. Input data are test data averaged from 29 to 30 sec, except as noted.

4. Site and normalized data were computed using the Rocketdyne PAST 640 modification zero computer program.

appendix III Instrumentation

The instrumentation for AEDC tests J4-1901-03 through J4-1901-06 is tabulated in Table III-1. The location of selected major engine instrumentation is shown in Fig. III-1.

TABLE III-1 INSTRUMENTATION LIST

AEDC Code	Parameter	Tap No.	Range	Mlero-	Magnetic Tape		rip X-Y
<u> </u>		110.		Baute	Tape	grapii Cr	art rioner
ICC	Current		amp				
	Control		0 to 30	x ,		*.	
nc, .	lgnition		0 to 30	x,		; x	
	Event		_			- (1	
EASIOV	Augmented Spark Igniter Oxidize Valve	r	Open/Cloaed	×		×	
EECL	Engine Cutoff Lockin		On/Off	x		×	
EECO	Engine Cutoff Signal		On/Off	x	x	x	
EES	Englne Start Command		On/Off	×		x	
EFBVC	Fuel Bleed Valve Closed Limit		Open/Closed	x			
EFPVC/O	Fuel Prevalve Closed/Open Limit	it	Closed/Open	×			
EHCS	Helium Control Solenoid		On/Off	×		x	
EID	Ignition Detected		On/Off	×		x	
EIPCS	Ignition Phase Control Solenoid		On/Off	x		x	
EMCS	Main-Stage Control Solenoid		On/Off	×		×	
EMP-1	Main-Stage Pressure No. 1		On/Off	×		x '	
EMP-2	Main-Stage Pressure No. 2		On /Off	×		×	
EOBVC	Oxidizer Bleed Valve Closed Lin	nit	Open/Closed	x			
EOPVC	Oxldizer Prevalve Closed Limit		Cloaec	x		×	
EOPVO	Oxidizer Prevalve Open Limit		Open	x		x	
ESTDCS	Start Tank Discharge Control So	lenoid	On/Off	x	×	x	
RASIS-1	Augmented Spark Igniter No. 1		On/Off			×	
RASIS-2	Augmented Spark igniter No. 2		On/Off			×	
RGGS-1	Gas Generator Spark No. 1		On/Off			×	
RGGS-2	Gas Generator Spark No. 2		On/Off			x	
	Flowa		gpm				
QF-1A	Fuel	PPF	0 to 9000	×		×	
QF-2	Fuel	PFFA	0 to 9000	×	×	×	
QF-1SAM	Fuel Flow Stall Approach Monitor		0 to 9000	×		×	
QFRP	Fuel Recirculation		0 to 160	×			
QO-1A	Oxidizer	POF	0 to 3000	x		x	
QO-2	Oxidizer	POFA	0 to 3000	×	x	×	
QORP	Oxidizer Recirculation		0 to 50	×			
	Position		Percent Open				
LFVT	Main Fuel Valve		0 to 100	×		×	
LGGVT	Gas Generator Valve		0 to 100	×		x	
LOTBVT	Oxldizer Turbine Bypasa Valve		0 to 100	×		×	
LOVT	Main Oxidizer Valve		0 to 100	×		x	
LPUTOP	Propellant Utilization Valve		0 to 100	×		x	x
LSTDVT	Start Tank Discharge Valve		0 to 100	x		x	

TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Micro- sadic	Magnetic Tape	Oscillo- graph	Strip Chart	X-Y Plotter
	Pressure		psia					
PA:	Test Cel:		0 to 0.5	×		×		
PA2	Test Ceil		0 to 1.0	x	x			•
PA3	Test Cal		U to 5. 0	x			×	
PC-1P	Thrust Chamber	CGı	0 to 1000	×				
PC-3	Thrust Chamber	CG:A	0 to :000	x	×	×		
PCBO-1	Constant Bleed Orifice		0 to 50	×				•
PCDP	Crossover Duct Purge		0 to 100	×				
PCGG-1P	Gas Generator Chamber		0 to 1000	×	×	×		
PCGG-2	Gas Generator Chamber	GG1A	0 to ±000	x				
PFBL	Fuel Bleed Line		0 to 500 ¹	×		×		
PFJ-1A	Main Fuel Injection	CF2	0 to 1000	×		×		
PFJGG-1A	Gas Generator Fuel Injection	GF4	0 to 1000	×		×		-
PFJGG-2	Gas Generator Fuel Injection	GF4	0 to 1000	x		×		
PFPC-1A	Fuel Pump Balance Piston Cavity	PF5	0 το 1000	x				
PFPD-1P	Fuel Pump Discharge	PF3	0 to 1500	x			•	
PFPD-2	Fuel Pump Discharge	PF2	0 to 1500	x	×	×		
PFPI-1	Fuel Pump Inlet		0 to 100	×		×		×
PFPI-2	Fuel Pump Iniet		0 to 100	x ·		×		x
PFPI-3	Fuel Pump Inlet		0 to 200		×			
PFPPSD-1	Fuel Pump Primary Seal Drain		0 to 200	×				
PFRPO	Fuel Recirculation Pump Outlet		0 to 60	x				
PFRPR	Fuel Recirculation Pump Return		0 to 50	×				
PFST-1P	Fuel Start Tank	TF1	0 to 1500	x		×		
PFST-2	Fuel Start Tark	TF1	0 to 1500	x				×
PFUT	Fuel Tank Ullage		0 to 100	x				•
P7VI	Fuel Tank Pressurization Line Nozzle Inlet		0 to 1000	x				•
PFVL	Fuel Tank Pressurization Line Nozzle Throa:		0 to 1000	x				
PHECMO	Pneumatic Control Module Outlet		0 to 750	x				
PHEOP	Oxidizer Recirculation Pump Purge		0 το 150	×				
PHET-1P	Helium 'fack	NN1	0 to 3500	×		x		
PHFT-2	Helium Tank	NN1	0 to 3500	×				×
PHRO-1A	Helium Regulator Outlot	NN2	0 to 750	x				
POJ-1A	Main Oxidizer Injection	CO3	0 to 1000	x		x		
POJ-2	Main Oxidizer Injection	CO3A	0 to 1000	x		x		
POJ-3	Main Oxidizer Injection		0 to 2000		x			
POJGG-1A	Gas Generator Oxidizer Injection	GO5	0 to 1000	×		x		
POJGG-2	Gas Generator Oxidizer Injection	GO5	0 to 1000	x				
POPBC-1A	Oxidizer Pump Bearing Coolant	PO7	0 to 500	×				

TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Micro- sadic	Magnetic Tape	Oscillo- graph	Strip Chart	X-Y Piotter
	Pressure		psia					
POPD-1P	Oxidizer Pump Discharge	PO3	0 to 1500	×				
POPD-2	Oxidizer Pump Discharge	PO2	0 to 1500	×	×	x		
POPI-1	Oxidizer Pump Inlet		0 to 100	x				×
POPI-2	Oxidizer Pump Inlet		0 to 200	×				×
POP1-3	Oxidizer Pump Inlet		0 to 100			×		
POPSC-IA	Oxidizer Pump Primary Seal Cavity	PO6	0 to 50	x				
PORPO	Oxidizer Recirculation Pump Outlet		0 to 115	x				
PORPR	Oxidizer Recirculation Pump Return		0 to 100	×				
POTI-1A	Oxidizer Turbine Inlet	TG3	0 to 200	×				
POTO-1A	Oxidizer Turbine Outlet	TG4	0 to 100	x				
POUT	Oxidizer Tank Uliage		0 to 100	x				
POVCC	Main Oxidizer Valve Closing Control		0 to 500	×				
POVI	Oxidizer Tank Pressurization Line Nozzle Inlet		0 to 1000	x				
POVL	Oxidizer Tank Presaurization Line Nozzle Throat		0 to 1000	x				
PPUVI-IA	Propellant Utilization Valve Inlet	PO8	0 to 1500	×				
PPUVO-1A	Propeilant Utilization Valve Outiet	PO9	0 to 500	x				
PTCFJP	Thrust Chamber Fuel Jacket Purge		0 to 100	x				
PTCP	Thrust Chamber Purge		0 to 1000	x				
PTPP	Turbopump and Gas Generator Purge		0 to 250	x				
	Speeds		rpm					
NFP-iP	Fuei Pump	PFV	0 to 30, 000	×	×	×		
NFRP	Fuel Recirculation Pump		0 to 15,000	x				
NOP-1P	Oxidizer Pump	POV	0 to 12,000	x	×	x		
NORP	Oxidizer Recirculation Pump		0 to 15,000	×				
	Temperatures		• F					
TA1	Teat Cell (North)		-50 to +800	x				
TA2	Test Cell (East)		-50 to +800	x				
TA3	Test Cell (South)		-50 to +800	×				
TA4	Teat Cell (West)		-50 to +800	×				
TAIP-IA	Auxiliary Instrument Package		-300 to +200	x				
TAIPAA	Auxiliary Instrument Package Area Ambient		-200 to +500	x				
TCDP	Crosaover Duct Purge		-i50 to +i50	×				
TECP-1P	Electrical Controls Package	NST 1A	-300 to +200	×			x	
ТЕНАА	Engine Handler Attach Area Ambien.		-200 to +500	x				

TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Micro-	Magnetic Tape	Oacıllo- graph	Strip Chart	X-Y Plotter
	Temperatures		<u>•</u> F					
TFAS1L-2	Augmented Spark Igniter Fuel Line Skin		-400 to +300	x				
TFAS1L-4	Augmented Spark Igniter Fuel Line Skin		-425 to +500	x ,				•
TFBV-1A	Fuel Bleed Valve	GFT1	-425 to -375	×				
TFD-1	Fire Detection		0 to 1000	x			x	
TFDAA	Fuc. High Pressure Duct Area Ambient		-200 to +500	x				
TFJ-1P	Main Fuel Injection	CFT2	-425 to +250	x		x		
TFJ-2 ²	Main Fuel Injection		-450 to +250	x				
TFPD-1P	Fuel Pump Discharge	PFT1	-425 to -400	x	x	x		•
TFPD-2	Fuel Pump Discharge	PFT1	-425 to -400	×				
TFP1-1	Fuel Pump Inlet		-425 to -400	x				x
TFP1-2	Fuel Pump Inlet		-425 to -400	×				x
TFRPO	Fuel Recirculation Pump Outlet		-425 to -350	×				
TFRPR	Fuel Recirculation Pump Return Line		-425 to -250	x				•
TFRT-1	Fuel Tank		-425 to -410	x				
TFRT-3	Fuel Tank		-425 to -410	×				-
TFST-1P	Fuel Start Tank	TFT1	-350 to +100	x				
TFST-2	Fuel Start Tank	TFT1	-350 to +100	×				x
TFTD-2	Fuel Turbine Discharge Duct		-200 to -1000	x			×	
TFTD-3	Fuel Turbine Discharge Duct		-200 to +1000	x			×	
TFTD-4	Fuel Turbine Discharge Duct		-200 to +1000	x			x ²	
TFTD-8	Fuel Turbine Discharge Duct		-200 to +1400	x			×	
TFTO .	Fuel Turbine Outlet	TFT2	0 to 1800	×				
TFTSD-1	Fuel Turbine Seal Drain Line		-300 to +100	×				
TGGO-1A and	2 Gas Generator Outlet	GGT1	0 to 2500	x		x	x	
TGGVRS	Gas Generator Valve Retaining Screw		-100 to +100	×			x3	
THET-1P	Helium Tank	NNTI	-350 to +100	x				x
TNODP	Oxidizer Dome Purge		0 to +300	×				
TOAS1L-1	Augmented Spark Igniter Oxidizer Line Skin		-425 to -500	x				
TOAS1L-2	Augmented Spark Igniter Oxidizer Line Skin		-400 to +300	ж				'
TOBS-1	Oxldizer Bootstrap Line		-300 to +250	x				
TOBS-2	Oxidizer Bootatrap Line		-300 to +250	x				
TOBS-2B	Oxicizer Bootstrap Line		-300 to +250	x				
TOBV-1A	Oxidizer Bleed Valve	GOT2	-300 to -250	x				
TODAA	Oxidizer Dome Area Ambient		-200 to +500	×				
TODS-1	Oxidizer Dome Skin		-300 to +100	x			x	
TODS-2	Oxidizer Dome Skin		-300 to +100	x			×4	

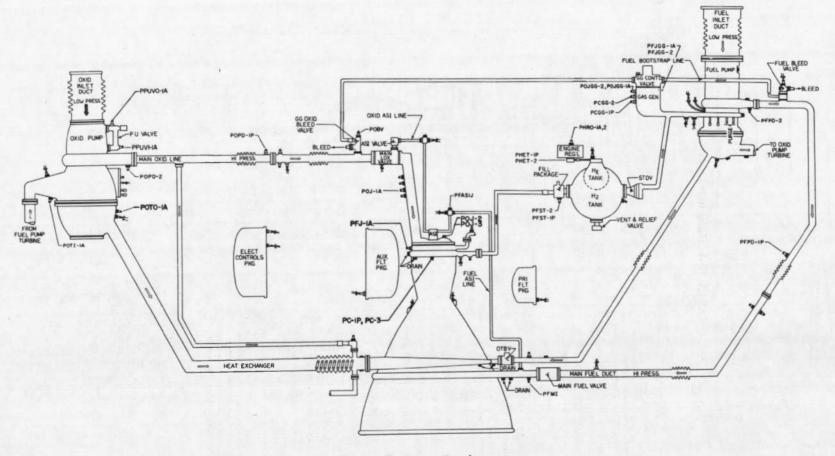
TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Micro-	Magnetic Tape	Oscillo- graph	Strip X-Y Chart Plotter
	Temperaturea		*F				
TOPB-1A	Oxidizer Pump Bearing Coolant	POT4	-300 to -250	x			
TOPD-1P	Oxidizer Pump Discharge	POT3	-300 to -250	x	×	×	x
TOPD-2	Oxidizer Pump Diacharge	POT3	-300 to -250	×			
TOPI-1	Oxidizer Pump Inlet		-310 to -270	x			x
TOP1-2	Oxidizer Pump Inlet		-310 to -270	×			x
TORPO	Oxidizer Recirculation Pump Outlet		-300 to -250	×			
TORPR	Oxidizer Recirculation Pump Return		-300 to -140	x			
TORT-1	Oxidizer Tank		-300 to -287	x			
TORT-1B	Oxidizer Tank		-300 to -287	x			
TORT-3	Oxidizer Tank		-300 to -287	x			
TOTI-1P	Oxidizer Turbine Inlet	TGT3	-300 to 1200	x			x
TOTO-1P	Oxidizer Turbine Outlet	TGT4	0 to 1000	x			
TOVL	Oxidizer Tank Pressurization Line Nozzle Throat		-300 to +100	x			
TPIP-1P	Primary instrument Package		-300 to +200	x			
TPIPAA	Primary Instrument Package Area Ambient		-200 to +500	x			
TSC2-1	Thruat Chamber Skin		-300 to +500	×			
TSC2-12	Thrust Chamber Skin		-300 to +500	x			
TSC2-13	Thrust Chamber Skin		-300 to +500	×			x
TSC2-17	Thrust Chamber Skin		-300 to +500	x			
TSC2-20	Thruet Chamber Skin		-300 to +500	×			
TSC2-24	Thruat Chamber Skin		-300 to +500	x			
TSOVC-1	Oxidizer Valve Actuator Cap		-325 to +150	x			x
TSTDVAA	Start Tank Diacharge Valve Area Ambient		-200 to +500	x			
TST DVDL	Start Tank Discharge Valve Drain Line		-100 to +200	x	•		
TSTDVOC	Start Tank Diacharge Valve Opening Control Port		-300 to +200	×	•		_× 3
TTC-1P	Thrust Chamber Jacket (Control)	CS1	-425 to +500	x			x
TTC-2	Thrust Chamber Jacket		-425 to +100	x			
TTCP ⁵	Thrust Chamber Purge		-345 to -504	x			
TTPP	Turbopump Purge		-150 to +150	x			x

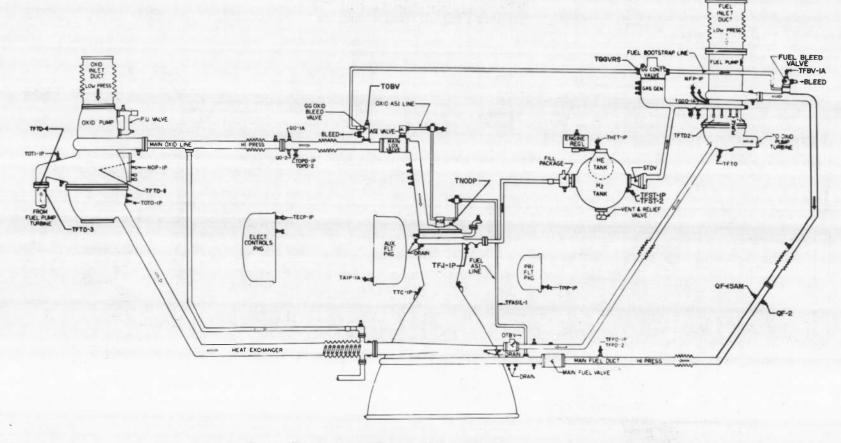
TABLE III-1 (Concluded)

AEDC	_000.00	Тар		Micro-	Magnetic	Oscillo-	Strip	X-Y
Code	Parameter	No.	Range	sadic	Tape	graph	Char:	Plotter
	Vibrations		g'a					
UAS1F-1	Augmented Spark Igniter Fuel Orifice Block Tangential		±150	x				
UASIV-1	Augmented Spark Igniter Oxidizer Valve Axial		±150	x				
UASIV-3	Augmented Spark Igniter Oxidizer Valve Tangential		±150	x				
UFPR	Fuel Pump Radial 90 deg		±300		x	x		
UMFV-1	Mair. Fuel Valve Radial		±150	x				
UMFV-3	Main Fuel Valve Tangential		±150	×				
UOPR	Oxidizer Pump Radial 90 deg		±200	x				
UOTBV-1	Oxidizer Turbine Bypass Valve Axial		±150		x			
UTCD-1	Thrust Chamber Dome		±500		x	x		
UTCD-2	Thrust Chamber Dome		±500		×	x		
UTCD-3	Thrust Chamber Dome		±500		x			
UTCD-4	Thrust Chamber Dome		±1000			x		
UIVSC	No. 1 Vibration Safety Counts		On/Off			x		
U2VSC	No. 2 Vibration Safety Counts		On/Off			×		
USVSC	No. 3 Vibration Safety Counts		On/Off			x		
	Voltage		volts					
VCB	Control Bus		0 to 36	x		x		
VIB	Ignition Bus		0 to 36	x		×		
VIDA	Ignition Detect Amplifier		9 to 16	x		x		
VPUTEP	Propellant Utilization Valve Excitation		0 to 5	x				

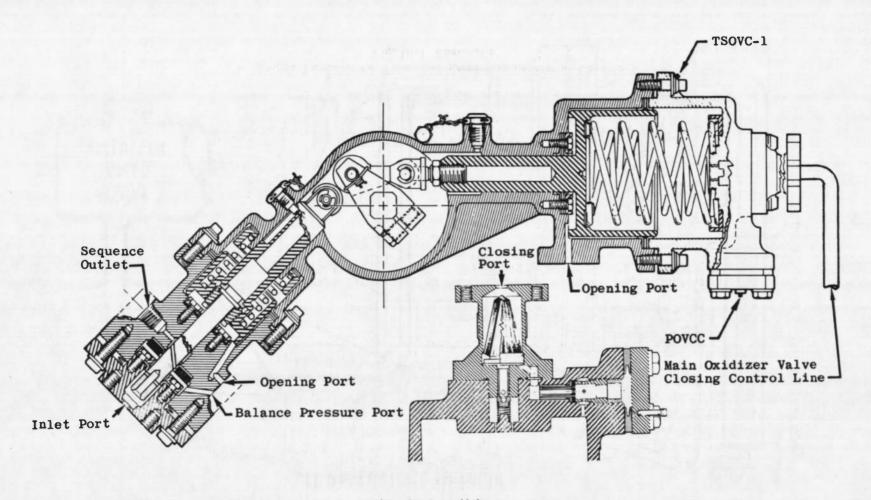
Notes: 1. Range changed from 0 to 100 psia beginning with test 04
2. Added beginning with test 04
3. Deleted beginning with test 05
4. Added beginning with test 05
5. Added beginning with test 06



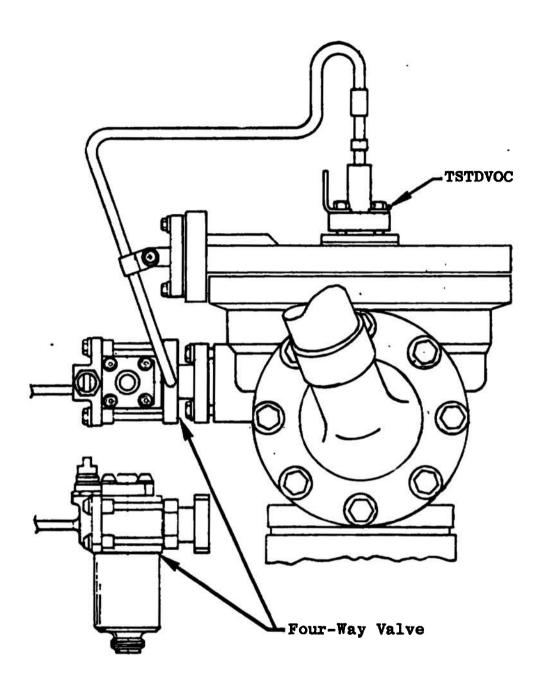
a. Engine Pressure Tap Locations Fig. III-1 Instrumentation Locations



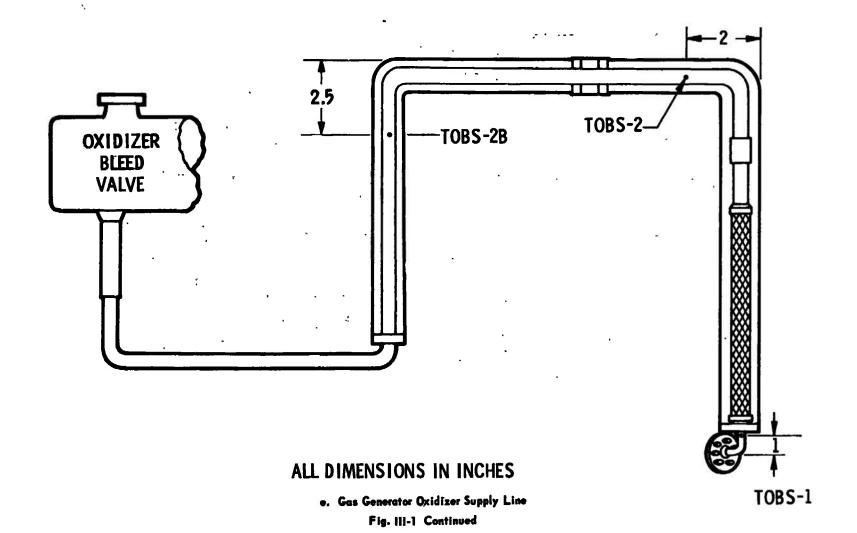
b. Engine Temperature, Flow, and Speed Instrumentation Locations
Fig. 111-1 Continued

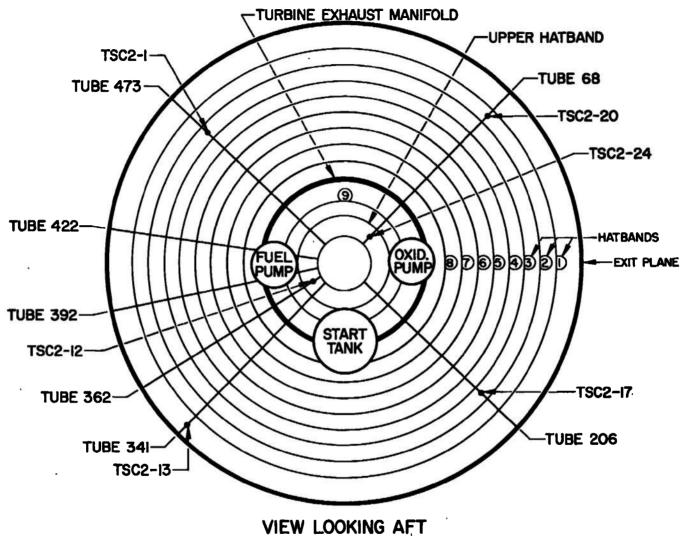


c. Main Oxidizer Valve Fig. III-1 Continued



d. Start Tank Discharge Valve Fig. III-1 Continued





f. Thrust Chambei

Fig. III-1 Concluded

APPENDIX IV METHOD OF CALCULATION (PERFORMANCE PROGRAM)

TABLE 17-1 PERFORMANCE PROGRAM DATA INPUTS

Item No.	Parameter					
1	Thrust Chamber (Injector Face) Pressure, psia					
2	Thrust Chamber Fuel and Oxidizer Injection Pressures, psia					
3	Thrust Chamber Fuel Injection Temperature, °F					
4 :	Fuel and Oxidizer Flowmeter Speeds, Hz					
<i>"</i> . ∴5	Fuel and Oxidizer Engine Inlet Pressures, psia					
55 1,6	Fuel and Oxidizer Pump Discharge Pressures, psia					
7	Fuel and Oxidizer Engine Inlet Temperatures, °F'					
8	Fuel and Oxidizer (Main Valves) Temperatures, *F					
9	Propellant Utilization Valve Center Tap Voltage, volts					
10	Propellant Utilization Valve Position, volts					
11	Fuel and Oxidizer Pump Speeds, rpm					
12	Gas Generator Chamber Pressure, psia					
13	Gas Generator (Bootstrap Line at Bleed Valve) Temperature, °F					
14	Fuel* and Oxidizer Turbine Inlet Pressure, psia					
15	Oxidizer Turbine Discharge Pressure, psia					
16	Fuel and Oxidizer Turbine Inlet Temperature, °F					
17	Oxidizer Turbine Discharge Temperature, °F					

*At AEDC, fuel turbine inlet pressure is calculated from gas generator chamber pressure.

NOMENCLATURE

Area, in.² Α В Horsepower C Coefficient C* Characteristic velocity, ft/sec Diameter, in. \mathbf{D} F Thrust, lbf Η Head, ft Enthalpy, Btu/lbm h I Impulse Molecular weight M Speed, rpm \mathbf{N} \mathbf{P} Pressure, psia Flow rate, gpm Q Resistance, sec²/ft³-in.² R Mixture ratio, O/F r Temperature, °F T TC* Theoretical characteristic velocity, ft/sec Weight flow, lb/sec \mathbf{W} \boldsymbol{z} Differential pressure, psi β Ratio Ratio of specific heats γ Efficiencies η θ Degrees Density, lb/ft³ ρ

SUBSCRIPTS

A Ambient

AA Ambient at thrust chamber exit

B Bypass nozzle

BIR Bypass nozzle inlet (Rankine)

BNI Bypass nozzle inlet (total)

C Thrust chamber

CF Thrust chamber, fuel

CO Thrust chamber, oxidizer

CV Thrust chamber, vacuum

E Engine

EF Engine fuel

EM Engine measured

EO Engine oxidizer

EV Engine, vacuum

e Exit

em Exit measured

F Thrust

FM Fuel measured

FV Thrust, vacuum

f Fuel

.G Gas generator

GF Gas generator fuel

GO Gas generator oxidizer

H1 Hot gas duct No. 1

H1R Hot gas duct No. 1 (Rankine)

H2R Hot gas duct No. 2 (Rankine)

IF Inlet fuel

IO Inlet oxidizer

ITF Isentropic turbine fuel

ITO Isentropic turbine oxidizer

N Nozzle

NB Bypass nozzle (throat).

AEDC-TR-68-238

NV Nozzle, vacuum

O Oxidizer

OC Oxidizer pump calculated

OF Outlet fuel pump

OFIS Outlet fuel pump isentropic

OM Oxidizer measured

OO Oxidizer outlet

PF Pump fuel

PO Pump oxidizer

PUVO Propellant utilization valve oxidizer

Calcius.

:

1. 1.

RNC Ratio bypass nozzle, critical

SC Specific, thrust chamber

SCV Specific thrust chamber, vacuum

SE Specific, engine

SEV Specific, engine vacuum

T Total

TEF Turbine exit fuel

TEFS Turbine exit fuel (static)

TF Fuel turbine

TIF Turbine inlet fuel (total)

TIFM Turbine inlet, fuel, measured

TIFS Turbine inlet fuel isentropic

TIO Turbine inlet oxidizer

TO Turbine oxidizer

t Throat

V Vacuum

v Valve

XF Fuel tank repressurant

XO Oxidizer tank repressurant

PERFORMANCE PROGRAM EQUATIONS

THRUST

Thrust Chamber, Vacuum

$$F_{CV} = C (P_C)^2 + B (P_C) + A$$

Empirical Determination from Curve Fit of Thrust versus P_C

Thrust Chamber

$$F_C = F_{CV} - P_{AA}A_e$$

$$A_e = A_{em} + 12.8$$

PAA = Measured Cell Pressure

Engine, Vacuum

$$F_{EV} = F_{CV}$$

Engine

$$F_E = F_C$$

MIXTURE RATIO

Engine

$$\mathbf{r_E} = \frac{\mathbf{W_{EO}}}{\mathbf{W_{EF}}}$$

$$W_{EO} = W_{OM} - W_{XO}$$

$$W_{EF} = W_{FM} - W_{XF}$$

Thrust Chamber

$$r_{C} = \frac{w_{CO}}{w_{CF}}$$

$$W_{CO} = W_{OM} - W_{XO} - W_{GO}$$

$$W_{CF} = W_{FM} - W_{XF} - W_{GF}$$

$$W_{GO} = W_{T} - W_{GF}$$

$$W_{GF} = \frac{W_{T}}{1 + r_{G}}$$

$$W_{T} = \frac{P_{TIF} A_{TIF} K_{7}}{TC*_{TIF}}$$

$$K_7 = 32.174$$

Normalized engine and thrust chamber vacuum data calculated as measured, except all flows are normalized using standard inlet pressures, temperatures, and densities listed below:

*: , 17...

10 -

$$P_{IO}$$
 STD = 39 psia

$$\rho_{IO} STD = 70.79 \text{ lb/ft}^3$$

$$\rho_{IF}$$
 STD = 4.40 lb/ft³

$$T_{IO}$$
 STD = -295.2°F

$$T_{IF} STD = 422.5 ^{\circ}F$$

SPECIFIC IMPULSE

Engine

$$I_{SE} = \frac{F_E}{W_E}$$

$$W_E = W_{EO} + W_{EF}$$

Engine, Vacuum

$$I_{SEV} + \frac{F_{EV}}{W_{FV}}$$

WEV = WE Normalized using standard inlet pressures, temperatures, and densities

Chamber

$$I_{SC} = \frac{F_C}{W_C}$$

$$W_{C} = W_{CO} + W_{CF}$$

Chamber, Vacuum

$$I_{SCV} = \frac{F_{CV}}{W_{CV}}$$

WCV = WC Normalized using standard inlet pressures, temperatures, and densities

CHARACTERISTIC VELOCITY

Thrust Chamber

$$C^* = \frac{K_7 P_C A_t}{W_C}$$

$$K_7 = 32,174$$

Thrust Chamber, Vacuum

$$C_{V}^{*} = \frac{K_{7} P_{CV} A_{t}}{W_{CV}}$$

$$K_7 = 32.174$$

- : Nozzle

003

$$C_N^* = \frac{C^*}{K_6}$$
 $K_6 = 1.086$

Nozzle, Vacuum

$$C_{NV}^* = \frac{C_V^*}{K_6}$$
 $K_6 = 1.086$

THRUST COEFFICIENT

Engine

$$C_{\mathbf{F}} = \frac{\mathbf{F}_{\mathbf{C}}}{\mathbf{P}_{\mathbf{C}}\mathbf{A}_{\mathbf{t}}}$$

Engine, Vacuum

$$C_{FV} = \frac{F_{CV}}{P_{C}A_{t}}$$

DEVELOPED PUMP HEAD

Oxidizer

$$H_0 = K_4 \left(\frac{P_{00}}{\rho_{00}} - \frac{P_{10}}{\rho_{10}} \right)$$
 $K_4 = 144$
 $\rho = \text{National Bureau of Standards Values f(P,T)}$

Fuel

$$H_F = 778.16 \Delta h_{OFIS}$$
 $\Delta h_{OFIS} = h_{OFIS} - h_{IF}$
 $h_{OFIS} = f(P,T)$
 $h_{IF} = f(P,T)$

Fuel and Oxidizer Vacuum

Conditions normalized using standard inlet pressures, temperatures, and densities.

PUMP EFFICIENCIES

Fuel, Isentropic

$$\eta_{\rm F} = \frac{h_{\rm OFIS} - h_{\rm IF}}{h_{\rm OF} - h_{\rm IF}}$$

$$h_{OF} = f(P_{OF}, T_{OF})$$

Oxidizer, Isentropic

$$\eta_{OC} = K_{40} \left(\frac{Q_{PO}}{N_{O}}\right)^{2} + K_{50} \left(\frac{Q_{PO}}{N_{O}}\right) + K_{60}$$

$$Y_{O} = 1.000$$

$$K_{40} = -5.053 \quad K_{50} = 3.861 \quad K_{60} = 0.0733$$

TURBINES

Oxidizer, Efficiency

$$\eta_{TO} = \frac{B_{TO}}{B_{ITO}} \\
B_{TO} = K_5 \frac{W_{PO} H_0}{\eta_0} \\
K_5 = 0.001818 \\
W_{PO} = W_{OM} + W_{PUVO} \\
W_{PUVO} = \sqrt{\frac{Z_{PUVO} \rho_{OO}}{R_v}} \\
Z_{PUVO} = A + B (P_{OO}) \\
A = -1597 \\
B = 2.3828 \\
if P_{OO} \ge 1010 \\
set P_{OO} = 1010$$

$$\ell_{n} R_{v} = A + B \left(\theta_{PUVO}\right) + C(\theta_{PUVO})^{3} + D (e)$$

$$+ E \theta_{PUVO} (e) \frac{\theta_{PUVO}}{7} + F \left[e \frac{\theta_{PUVO}}{7} \right]^{2}$$

٠٠,

$$A = 5.566 \times 10^{-1}$$

$$B = 1.500 \times 10^{-2}$$

$$C = 7.941 \times 10^{-6}$$

$$D = 1.234$$

$$E = -7.255 \times 10^{-2}$$

$$F = 5.069 \times 10^{-2}$$

Fuel, Efficiency

$$\eta_{\rm TF} = \frac{B_{\rm TF}}{B_{\rm ITF}}$$

$$B_{ITF} = K_{10} \Delta h_F W_T$$

$$\Delta h_F = h_{TIF} - h_{TEF}$$

$$B_{TF} = B_{PF} = K_5 \left(\frac{W_{PF} H_F}{\eta_F}\right)$$

$$W_{PF} = W_{FM}$$

$$K_{10} = 1.415$$

$$K_5 = 0.001818$$

Oxidizer, Developed Horsepower

$$B_{PO} = K_5 \left(\frac{W_{PO} H_0}{\eta_0} \right)$$

$$K_5 = 0.001818$$

 $B_{TO} = B_{PO}$

Fuel, Developed Horsepower

$$B_{TF} = B_{PF}$$

$$B_{PF} = K_5 \left(\frac{W_{PF} H_F}{\eta_F} \right)$$

$$W_{PF} = W_{FM}$$

Fuel, Weight Flow

$$W_{TF} = W_{T}$$

$$W_{TO} = W_{T} - W_{B}$$

$$W_{B} = \begin{bmatrix} \frac{2K_{7} & \gamma_{H2}}{\gamma_{H2} - 1} & (P_{RNC}) & \frac{\gamma_{H2}}{\gamma_{H2}} \end{bmatrix}^{\frac{1}{2}} \begin{bmatrix} 1 - (P_{RNC}) & \frac{\gamma_{H2} - 1}{\gamma_{H2}} \end{bmatrix}^{\frac{1}{2}} & \frac{A_{NB} & P_{BNI}}{(R_{H2}, T_{BIR})^{\frac{1}{2}}} \\ P_{RNC} = f & (\beta_{NB}, \gamma_{H2}) \\ \beta_{NB} = D_{NB}/D_{B} \\ \gamma_{H2}, & M_{H2} = f(T_{H2R}, r_{G}) \\ A_{NB} = K_{13} & (D_{NB})^{2} \\ K_{13} = 0.7854 \\ T_{BIR} = T_{TIO} + 460 \\ P_{BNI} = P_{TEFS} \\ P_{TEFS} = Iteration of P_{TEF}$$

$$P_{TEF} = P_{TEFS} \left[1 + K_8 \left(\frac{W_T}{P_{TEFS}} \right)^2 \frac{T_{H2R}}{D^4_{TEF} M_{H2}} \left(\frac{\gamma_{H2} - 1}{\gamma_{H2}} \right) \right] \frac{\gamma_{H2}}{\gamma_{H2} - 1}$$

$$K_8 = 38.90$$

GAS GENERATOR

Mixture Ratio

$$r_G = D_1 (T_{H1})^3 + C_1 (T_{H1})^2 + B_1 (T_{H1}) + A_1$$

$$A_1 = 0.2575 \stackrel{3}{=} f \cdot \cdot \cdot f \qquad ...$$

$$B_1 = 5.586 \times 10^{-4}$$

$$C_1 = -5.332 \times 10^{-9}$$

$$D_1 = 1.1312 \times 10^{-11}$$

$$T_{H1} = T_{TIFM}$$

Flows

$$TC*_{TIF} = D_{2} (T_{H1})^{3} + C_{2} (T_{H1})^{2} + B_{2} (T_{H1}) + A_{2}$$

$$A_{2} = 4.4226 \times 10^{3}$$

$$B_{2} = 3.2267$$

$$C_{2} = -1.3790 \times 10^{-3}$$

$$D_{2} = 2.6212 \times 10^{-7}$$

$$P_{TIF} = P_{TIFS} \left[1 + K_{8} \left(\frac{W_{T}}{P_{TIFS}} \right)^{2} \frac{T_{H1R}}{D^{4}_{TIF} M_{H1}} \frac{\gamma_{H1} - 1}{\gamma_{H1}} \right]^{\frac{\gamma_{H1} - 1}{\gamma_{H1} - 1}}$$

$$K_{8} = 38.8983$$

Note: PTIF is determined by iteration.

$$T_{H1R} = T_{T1FM} + 460$$

$$M_{H1}$$
, γ_{H1} , C_p , $r_{H1} = f (T_{H1R}, r_G)$

Security Classification								
DOCUMENT CONTROL DATA - R & D								
(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)								
Arnold Engineering Development Center			NCLASSIFIED N/A					
ARO, Inc., Operating Contractor Arnold Air Force Station, Tennessee								
3. REPORT TITLE								
FLIGHT SUPPORT TESTING OF THE J-2 ROCKET ENGINE IN PROPULSION ENGINE TEST CELL (J-4) (TESTS J4-1901-03 THROUGH J4-1901-06)								
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) July 23 through August 15, 1968 - Interim Report								
5. AUTHOR(5) (First name, middle initial, last name)								
N. R. Vetter, ARO, Inc.								
6. REPORT DATE	78. TOTAL NO. OF	PAGES	7b. NO. OF REFS					
pecemper 1909	161 4							
54. CONTRACT OR GRANT NO. F40600-69-C-0001	90. ORIGINATOR'S REPORT NUMBER(S)							
b. PROJECT NO. 9194	AEDC-TR-68-238							
^c System 921E	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)							
d.	N/A							
10. DISTRIBUTION STATEMENT								
Each transmittal of this document outside the Department of Defense mushave prior approval of NASA, Marshall Space Flight Center (L-E-J),								
Huntsville, Alabama 35812.								
T. SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY							
	NASA, Marshall Space Flight							
Available in DDC.	Center (I-E-J),							
Carlotte Section 1	Huntsville, Alabama 35812							
Fourteen firings of the Rocketdyne J-2 rocket engine (S/N J-2036-1 were conducted at pressure altitude conditions during four test periods (J4-1901-03 through J4-1901-06) between July 23 and August 15, 1968, in Test Cell J-4 of the Large Rocket Facility. This testing was in support of the J-2 engine application to the S-II and S-IVB stages of								
the Column Washington was a second in the day and a second								

Fourteen firings of the Rocketdyne J-2 rocket engine (S/N J-2036-1) were conducted at pressure altitude conditions during four test periods (J4-1901-03 through J4-1901-06) between July 23 and August 15, 1968, in Test Cell J-4 of the Large Rocket Facility. This testing was in support of the J-2 engine application to the S-II and S-IVB stages of the Saturn V vehicle. The firings were accomplished at pressure altitudes between 78,000 and 110,000 ft at engine start. The primary objective of these firings was to evaluate engine start transients under various combinations of starting conditions with start tank energy being the major variable. The total accumulated firing duration for these four test periods was 223.2 sec.

This document is subject to special export controls and each transmittal to foreign governments or foreign nationals may be made only with prior approval of NASA, Marshall Space Flight Center (I-E-J), Huntsyille, Alabama 35812

This document has been approved for public release, its distribution is unlimited. Per Affective delay.

UNCLASSIFIED Security Classification LINK C 14. LINK A LINK B KEY WORDS ROLE ROLE ROLE J-2 rocket engines liquid propellants altitude simulation flight simulation startup performance tests performance evaluation 1. Rochet moters -- J-2 AFS. A- HIS AFS TORS